# The GLUEX Beamline and Detector

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# 70 Abstract

The GLUEX experiment at Jefferson Lab has been designed to study photoproduction reactions with a 9-GeV linearly polarized photon beam. The energy and arrival time of beam photons are tagged using a scintillator hodoscope and a scintillating fiber array. The photon flux is determined using a pair spectrometer, while the linear polarization of the photon beam is determined using a polarimeter based on triplet photoproduction. Charged-particle tracks from interactions in the central target are analyzed in a solenoidal field using a central straw-tube drift chamber and six packages of planar chambers with cathode strips and drift wires. Electromagnetic showers are reconstructed in a cylindrical scintillating fiber calorimeter inside the magnet and a lead-glass array downstream. Charged particle identification is achieved by measuring energy loss in the wire chambers and using the flight time of particles between the target and detectors outside the magnet. The signals from all detectors are recorded with flash ADCs and/or pipeline TDCs into memories allowing trigger decisions with a latency of  $3.3 \,\mu s$ . The detector operates routinely at trigger rates of 40 kHz and data rates of 600 megabytes per second. We describe the photon beam, the GLUEX detector components, electronics, data-acquisition and monitoring systems, and the performance of the experiment during the first three years of operation.

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# 156 1. The GlueX experiment

The search for Quantum ChromoDynamics (QCD) exotics uses data from 157 a wide range of experiments and production mechanisms. Historically, the 158 searches have looked for the gluonic excitations of mesons, searching for states 159 of pure glue, glueballs, and hybrid mesons where the gluonic field binding the 160 quark-anti-quark pair has been excited. Most experiments searching for glue-161 balls looked for scalar mesons [1], where the searches relied on over-population 162 of nonets, as well as unusual meson decay patterns. In the search for hybrid 163 mesons [2, 3], efforts have focused on particles with exotic quantum numbers, 164 i.e. systems beyond simple quark-anti-quark configurations. Good evidence 165

exists for an isospin 1 state, the  $\pi_1(1600)$ . Looking collectively at past studies, data from high-statistics photoproduction experiments in the energy range above 6 GeV are lacking.



Figure 1: (Color online)A cut-away drawing of the GLUEX detector in Hall D, not to scale.

The Gluonic Excitation (GLUEX) experiment at the US Department of En-169 ergy's Thomas Jefferson National Accelerator Facility (JLab)<sup>20</sup> has been built 170 to search for and map out the spectrum of exotic hybrid mesons using a 9-GeV 171 linearly-polarized photon beam incident on a proton target [4]. The GLUEX 172 detector and beamline are shown schematically in Figure 1. The detector is 173 nearly hermetic for both charged particles and photons arising from reactions 174 in the cryogenic target at the center of the detector, allowing for reconstruction 175 of exclusive final states. A 2-T solenoidal magnet surrounds the drift chambers 176 used for charged-particle tracking. Two electromagnetic calorimeters cover the 177 central and forward regions, and a scintillation detector downstream provides 178 particle-identification capability through time-of-flight measurements. 179

## 180 1.1. The Hall-D complex

The GLUEX experiment is housed in the Hall-D complex at JLab (see Fig.2). 181 This new facility starts with an extracted electron beam at the north end of the 182 Continuous Electron Beam Accelerator Facility (CEBAF) [5, 6]. The electron 183 beam is delivered to the Tagger Hall, where the maximum energy is 12 GeV, 184 due to one more pass through the north linac than the other experimental halls 185 (A, B and C). Here, linearly-polarized photons are produced through coherent 186 bremsstrahlung off a 50  $\mu$ m thick diamond crystal radiator. The scattered elec-187 trons pass through a tagger magnet and are bent into tagging detectors. A 188 high-resolution scintillating-fiber tagging array covers the 8 to 9 GeV energy 189

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Figure 2: (Color online) Schematic of the CEBAF accelerator showing the additions made during the 12-GeV project. The Hall-D complex is located at the north-east end.

range, and a tagger hodoscope covers photon energies both from 9 GeV to the 190 endpoint, and from 8 GeV to 3 GeV. Electrons not interacting in the diamond 191 are directed into a 60 kW electron beam dump. The tagged photons travel to 192 the Hall-D experimental hall. The distance from the radiator to the primary 193 collimator is 75 m. The collimator of 5 mm diameter removes off-axis incoherent 194 photons. The front face of the collimator is instrumented with an active colli-195 mator to aid in beam tuning. The beamline and tagging system are described 196 below in Section 2. 197

Downstream of the primary collimator is a thin beryllium radiator used by both the Triplet Polarimeter, which measures the linear polarization of the photons, and a Pair Spectrometer, which is used to measure the flux of the photons. More information on the production, tagging and monitoring of the photon beam can be found in Section 2. The photon beam continues through to a liquid hydrogen target at the heart of the GLUEX detector, and then to the end of the experimental hall where it enters the photon beam dump.

The layout of the GLUEX detector is shown in Fig. 3. The spectrometer is 205 based on a 4-m-long solenoidal magnet that is operated at a maximum field of 206 2 T, see Section 3. The liquid-hydrogen target is located inside the upstream 207 bore of the magnet. The target consists of a 2-cm-diameter, 30-cm-long vol-208 ume of hydrogen, as described in Section 4. Surrounding the target is the Start 209 Counter, which consists of 30 thin scintillator paddles that bend to a nose on 210 the down-stream end of the hydrogen target. The Start Counter is the primary 211 detector that registers the time coincidence of the radio-frequency (RF) bunch 212 containing the incident electron and the tagged photon producing the interac-213 tion. More information on this scintillator detector can be found in Section 8. 214

<sup>215</sup> The Central Drift Chamber, a cylindrical straw-tube detector, starts at a



Figure 3: GlueX spectrometer layout. Dimensions are given in mm. The numbers show the Z-coordinates of the detectors' centers, or of the front face of the FCAL modules. Glossary: SC - Start Counter (Section 8.1), CDC - Central Drift Chamber (Section 5.1), FDC - Forward Drift Chamber (Section 5.2), BCAL - Barrel Calorimeter (Section 7.1), TOF - Time-of-Flight hodoscope (Section 8.2), FCAL - Forward Calorimeter (Section 7.2).

radius of 10 cm from the beam line. The active volume of the chamber extends 216 from 48 cm upstream to 102 cm downstream of the target center, and from 217 10 cm to 56 cm in radius. The Central Drift Chamber consists of 28 layers of 218 straw tubes in axial and two stereo orientations. Downstream of the central 219 tracker is the Forward Drift Chamber, which consists of four packages, each 220 containing 6 planar layers in alternating u-y-v orientations. Both cathodes and 221 anodes in the Forward Drift Chamber are read out, providing three-dimensional 222 space point measurements. More details on the tracking system are provided in 223 Sections 5 and 6. 224

Downstream of the magnet is the Time-of-Flight wall. This system consists 225 of two layers of scintillator paddles in a crossed pattern, and, in conjunction with 226 the Start Counter, is used to measure the flight time of charged particles. More 227 information on the time-of-flight system is provided in Section 8. Photons aris-228 ing from interactions within the GLUEX target are detected by two calorimeter 229 systems. The Barrel Calorimeter, located inside the solenoid, consists of layers 230 of scintillating fibers alternating with lead sheets. The Forward Calorimeter is 231 downstream of the Time-of-Flight wall, and consists of 2800 lead-glass blocks. 232 More information on the the calorimeters can be found in Section 7. 233

# 234 1.2. Experimental requirements

The physics goals of the GlueX experiment require the reconstruction of ex-235 clusive final states. Thus, the GLUEX detector must be able to reconstruct both 236 charged particles  $(\pi^{\pm}, K^{\pm} \text{ and } p/\bar{p})$  and particles decaying into photons  $(\pi^{\circ}, \eta, \eta)$ 237  $\omega$  and  $\eta'$ ). For this capability, the charged particles and photons must be re-238 constructed with good momentum and energy resolution. The experiment must 239 also be able to reconstruct the energy of the incident photon (8 to 9 GeV) with 240 high accuracy (0.1%) and have knowledge of the linear polarization (maximum 241  $\sim 40\%$ ) of the photon beam to an absolute precision of 1%. Finally, many inter-242 esting final states involve more than five particles. Thus, the GLUEX detector 243 must also be nearly hermetic for both charged particles and photons, with an 244 acceptance that is reasonably uniform, well understood, and accurately modeled 245 in simulation. 246

In practice, the typical momentum resolution for charged particles is 1-3%, 247 while the resolution is 8-9% for very-forward high-momentum particles. For 248 most charged particles, the tracking system has nearly hermetic acceptance for 249 polar angles from  $1^{\circ} - 2^{\circ}$  to  $150^{\circ}$ . However, protons with momenta below about 250 250 MeV/c are absorbed in the hydrogen target and not detected. A further 251 challenge is the reconstruction of tracks from charged pions with momenta under 252 200 MeV/c due to spiraling trajectories in the magnetic field. The measurement 253 of energy loss (dE/dx) in the Central Drift Chamber enables the separation of 254 pions and protons up to about 800 MeV/c, while time-of-flight determination 255 allows separation of forward-going pions and kaons up to about 2 GeV/c. 256

For photons produced from the decays of reaction products, the typical energy resolution is 5 to  $6\%/\sqrt{E_{\gamma}}$ . Photons above 60 MeV can be detected in the Barrel Calorimeter, with some variation depending on the incident angle. The interaction point along the beam direction is determined by comparing the information from the readouts on the upstream and downstream ends of the detector. In the Forward Calorimeter, photons with energies larger than 100 MeV
can be detected with uniform resolution across the face of the detector. There
is a gap between the calorimeters at around 11°, where energy can be lost due
to shower leakage. Both photon detection efficiency and energy resolution are
degraded in this region.

#### 267 1.3. Data requirements

The physics analyses need to be carried out in small bins of energy and momentum transfer, necessitating not only the ability to reconstruct exclusive final states but also to collect sufficient statistics. While exact cross sections are not known, the cross sections of interest will be in the 10 nb to 1  $\mu$ b range.

This paper describes the operation of GLUEX Phase I. During this initial 272 phase, the GLUEX experiment has run with a data acquisition system capable of 273 collecting data using photon beams of a few  $10^7 \gamma/s$  in the coherent peak (8.4-9 274 GeV), with an expectation to run with 2.5 times higher rates in the future. The 275 data acquisition system ran routinely at 40 kHz with raw event sizes of 15-20 276 kilobytes, collecting about 600 megabytes of data per second. With firmware 277 improvements, future running is expected at 90 kHz and 1 gigabyte per second. 278 Details of the trigger and data acquisition are presented in Sections 9 and 10. 279

# 280 1.4. Coordinate system

For reference, we introduce here the overall experiment coordinate system, which is used in this document and throughout the analysis. The z-axis is defined along the nominal beamline increasing downstream. The coordinate system is right-handed with the y-axis pointing vertically up and the x-axis pointing approximately north. The origin is located 50.8 cm (20 inches) downstream of the upstream side of the upstream endplate of the solenoid, placing the nominal center of the target at (0,0,65 cm).

## 288 2. The coherent photon source and beamline

#### 289 2.1. CEBAF electron beam

CEBAF has a race track configuration with two parallel linear accelerators based on superconducting radio frequency (RF) technology [5]. The machine operates at 1.497 GHz and delivers beam to Hall D at 249.5 MHz.<sup>21</sup> Precise timing signals for the accelerator beam bunches are available to the experiment and are used to determine the time that individual photon bunches pass through the target. The nominal properties for the CEBAF electron beam to the Tagger Hall are listed in Table 1.

<sup>&</sup>lt;sup>21</sup>Hall D beam at 499 MHz is possible, but not the norm.

Table 1: Electron beam parameters. The emittance, energy spread and related parameters are estimates based on a model of the transport line from the accelerator to the Hall D radiator. The dimensions of the beam spot at the position of the radiator are directly measured, and vary around the stated values by  $\pm 30\%$  depending on beam conditions. Values for image size at collimator, obtained by projection of the electron beam spot convergence forward to the position of the primary photon collimator, have relative uncertainties of 50%.

parameter	design results
energy	$12 \mathrm{GeV}$
energy spread, RMS	$2.2 { m MeV}$
transverse $x$ emittance	$2.7 \text{ mm} \cdot \mu \text{rad}$
transverse $y$ emittance	$1.0 \text{ mm} \cdot \mu \text{rad}$
x spot size at radiator, RMS	$1.1 \mathrm{mm}$
y spot size at radiator, RMS	$0.7 \mathrm{mm}$
x image size at collimator, RMS	$0.5 \mathrm{mm}$
y image size at collimator, RMS	$0.5 \mathrm{~mm}$
image offset from collimator axis, RMS	$0.2 \mathrm{mm}$
distance radiator to collimator	$75.3 \mathrm{m}$

#### 297 2.2. Hall-D photon beam

The Hall-D complex, described in Section 1.1 and shown schematically in 298 Fig. 4, includes a dedicated Tagger Hall, an associated collimator cave, and 299 Experimental Hall D itself. A linearly-polarized photon beam is created using 300 the process of coherent bremsstrahlung [7, 8] when the electron beam passes 301 through an oriented diamond radiator at the upstream end of the Tagger Hall. 302 The electron beam position at the radiator is monitored and controlled using 303 beam position monitors (5C11 and 5C11B) which are located at the end of the 304 accelerator tunnel just upstream of the Tagger Hall (see Fig. 4.) The CEBAF 305 electron beam is tuned to converge as it passes through the radiator, ideally 306 so that the electron beam forms a virtual focus at the collimator located 75 m 307 downstream of the radiator. At the collimator, the virtual spot size of 0.5 mm 308 is small compared to the cm-scale size of the photon beam on the front face of 309 the collimator, such that a cut on photon position at the collimator is effectively 310 a cut on photon emission angle at the radiator. The convergence properties of 311 the electron beam are measured by scanning the beam profile with vertical and 312 horizontal wires. The wire scanners are referred to as "harps." Examples of the 313 horizontal and vertical convergence of the electron beam envelope (undeflected 314 by the tagger magnet) measured using harp scans and projected downstream 315 along the beamline are shown in Fig. 5. 316

The photon beam position on the collimator is monitored using an active collimator positioned just upstream of the primary photon beam collimator (described below in section 2.7). The position stability of the photon beam is maintained during normal operation by a feedback system that locks the position of the electron beam at the 5C11B beam position monitor and, consequently, the photon beam at the active collimator. The stability of the electron beam



Figure 4: Schematic layout of the Hall-D complex, showing the Tagger Hall, Hall D, and several of the key beamline devices. Also indicated are the locations of the 5C11B and AD00C beam monitors.



Figure 5: (Color online) Measurements of the root-mean-square width of the electron beam in horizontal (left) and vertical (right) projections as a function of position along the beamline, based on harp scans (data points) of the electron beam. The radiator position is just upstream of the third data point. The primary collimator position is marked by the vertical line indicated by the arrow. The curve downstream of the radiator is an extrapolation from the measured data points, with extrapolation uncertainty indicated by the shaded regions.

<sup>323</sup> current and position is monitored using an independent beam monitor (AD00C <sup>324</sup> in Fig. 4) located immediately upstream of the electron dump.

The linearly-polarized photon beam is produced via a radiator placed in the 325 electron beam just upstream of the Tagger (section 2.4). A properly aligned 326  $20-60\,\mu\mathrm{m}$  thick diamond crystal radiator produces linearly polarized photons 327 via coherent bremsstrahlung in enhancements [7, 8], that appear as peaks at 328 certain energies in the collimated bremsstrahlung intensity spectrum (Fig. 6), 329 superimposed upon the ordinary continuum bremsstrahlung spectrum from an 330 aluminum radiator. The energies of the coherent photon peaks and the degree 331 of polarization in each of those peaks depend on the crystal orientation with 332 respect to the incident electron beam. Adjustment of the orientation of the 333 diamond crystal with respect to the incoming electron beam permits production 334 of essentially any coherent photon peak energy up to that of the energy of the 335



Figure 6: (color online) (a) Collimated photon beam intensity versus energy as measured by the Pair Spectrometer. (b) Collimated photon beam polarization as a function of beam energy, as measured by the Triplet Polarimeter, with data points offset horizontally by  $\pm 0.015$  GeV for clarity. The labels PARA and PERP refer to orientations of the diamond radiator that result in polarization planes that are parallel and perpendicular to the horizontal, respectively.

incident electron beam, as well as the degree or direction of linear polarization.
A choice of 9 GeV for the primary peak energy, corresponding to 40% peak
linear polarization, was found to be optimum for the GLUEX experiment with
a 12-GeV incident electron beam.

The degree of polarization for a coherent bremsstrahlung beam is great-340 est for photons emitted at small angles with respect to the incident electron 341 direction. Collimation of the photon beam to a fraction of the characteristic 342 bremsstrahlung angle exploits this correlation to significantly enhance the aver-343 age polarization of the beam. In the nominal GLUEX beamline configuration, 344 a 5.0-mm-diameter collimator  $^{22}$  positioned 75 m downstream of the radiator is 345 used, corresponding to a cut at approximately 1/2 m/E in characteristic angle, 346 where m is the electron rest mass and E is the energy of the incident elec-347 tron. The photon beam energy spectrum and photon flux after collimation are 348 measured by the Pair Spectrometer (section 2.10), located downstream of the 349 collimator in Hall D. 350

An example of the measured photon spectrum and degree of polarization with a 12-GeV electron beam is shown in Fig. 6. The spectrum labeled "Aluminum" in Fig. 6(a) shows the spectrum of ordinary (incoherent) bremsstrahlung, normalized to the approximate thickness of the diamond radiator in terms of radiation lengths. The expected degree of linear polarization in the energy range of 8.4–9.0 GeV is  $\sim 40\%$  after collimation. The photon beam polariza-

 $<sup>^{22}{\</sup>rm A}$  3.4 mm collimator is also available, and has been used for some physics production runs with the thinnest (20  $\mu m)$  diamond.

Table 2: Typical parameters for the GLUEX photon beam, consistent with the electron beam properties listed in Table 1, a diamond radiator of thickness 50  $\mu$ m, and the standard primary collimator of diameter 5.0 mm located at the nominal position. The electron beam current incident on the radiator is taken to be 150 nA. The hadronic rates are calculated for the GLUEX 30 cm liquid hydrogen target.

E upper edge of the coherent peak	9 GeV
Coherent peak effective range	$8.4$ - $9.0~{\rm GeV}$
Net tagger rate in the coherent peak range	$45 \mathrm{~MHz}$
$N_{\gamma}$ in the peak range after collimator	$24 \mathrm{~MHz}$
Maximum polarization in the peak, after collimator	40%
Mean polarization in the peak range, after collimator	35%
Power absorbed on collimator	$0.60 \mathrm{W}$
Power incident on target	$0.23 \mathrm{W}$
Total hadronic rate	$70 \mathrm{~kHz}$
Hadronic rate in the peak range	$3.7~\mathrm{kHz}$

tion is directly measured by the triplet polarimeter (section 2.9) located just upstream of the pair spectrometer. The stability of the beam polarization is independently monitored via the observed azimuthal asymmetry in various photoproduction reactions, particularly that for  $\rho$  photoproduction [9].

Typical values for parameters and properties of the photon beam are given in Table 2. In the sections that follow, we describe in more detail how the linearlypolarized photon beam is produced, how the photon energy is determined using the tagging spectrometer, how the photon beam polarization spectrum and flux are measured with the Pair Spectrometer and Triplet Polarimeter, and how the photon flux is calibrated using the Total Absorption Counter.

#### 367 2.3. Goniometer and radiators

For the linearly-polarized photon beam normally used in GLUEX produc-368 tion running, diamond radiators are used to produce a coherent bremsstrahlung 369 beam. This requires precise alignment of the diamond radiator, in order to 370 produce a single dominant coherent  $peak^{23}$  with the desired energy and polar-371 ization by scattering the beam electrons from the crystal planes associated with 372 a particular reciprocal lattice vector. A multi-axis goniometer, manufactured by 373 Newport Corporation, precisely adjusts the relative orientation of the diamond 374 radiator with respect to the incident electron beam horizontally, vertically and 375 rotationally about the X, Y and Z axes, respectively. The Hall-D goniometer 376 holds several radiators, any of which may be moved into the beam for use at 377 any time according to the requirements of the experiment. 378

In addition to the diamond radiators, several aluminum radiators of thicknesses ranging from 1.5 to  $40 \ \mu m$  are used to normalize the rate spectra measured

 $<sup>^{23}</sup>$ Defined as 0.6 GeV below the coherent edge (nominally 9 GeV). The position of the edge scales approximately with the primary incident electron beam energy.

in the Pair Spectrometer, correcting for its acceptance. A separate rail for these
 amorphous radiators is positioned 615 mm downstream of the goniometer.

## 283 2.3.1. Diamond selection and quality control

The properties of diamond are uniquely suited for coherent bremsstrahlung 384 radiators. The small lattice constant and high Debye temperature of diamond 385 result in an exceptionally high probability for coherent scattering in the brems-386 strahlung process [10]. Also, the high coherent scattering probability is a conse-387 quence of the small atomic number of carbon (Z = 6). At the dominant crystal 388 momentum (9.8 keV) corresponding to the leading (2.2.0) reciprocal lattice vec-389 tor, the small atomic number results in minimal screening of the nuclear charge 390 by inner shell electrons. Diamond is the best known material in terms of its 391 coherent radiation fraction, and its unparalleled thermal conductivity and ra-392 diation hardness make it well-suited for use in a high-intensity electron beam 393 environment. 394

The position of the coherent edge in the photon beam intensity spectrum is 395 a simple monotonic function of the angle between the incident electron beam 396 direction and the normal to the (2,2,0) crystal plane. The 12-GeV-electron 397 beam entering the radiator has a divergence less than 10  $\mu$ rad, corresponding 398 to a broadening of the coherent edge in Fig. 6 by just 7 MeV. However, if the 399 incident electron beam had to travel through 100  $\mu$ m of diamond material prior 400 to radiating, the resulting electron beam emittance would increase by a factor 401 of 10 due to multiple Coulomb scattering, resulting in a proportional increase in 402 the width of the coherent edge. Such broadening of the coherent peak diminishes 403 both the degree of polarization in the coherent peak as well as the collimation 404 efficiency in the forward direction. Hence, diamond radiators for GLUEX must 405 be significantly thinner than 100 microns. 406

The cross-sectional area of a diamond target must also be large enough to 407 completely contain the electron beam so that the beam does not overlap with 408 the material of the target holder. Translated to the beam spot dimensions from 409 Table 1, GLUEX requires a target with transverse size 5 mm or greater. Uniform 410 single-crystal diamonds of this size are now available as slices cut from natural 411 gems, HPHT (high-pressure, high-temperature) synthetics, and CVD (chemical 412 vapor deposition) single crystals. Natural gems are ruled out due to cost. HPHT 413 crystals had been thought to be far superior to CVD single crystals in terms 414 of their diffraction widths, but our experience did not bear this out. GLUEX 415 measurements of the x-ray rocking curves of CVD crystals obtained from the 416 commercial vendor Element Six<sup>24</sup> routinely showed widths that were within a 417 factor 2 of the theoretical Darwin width, similar to the results we found for the 418 best HPHT diamonds that were available to us [11, 12]. 419

Fig. 7 shows a rocking curve topograph of a diamond radiator taken with 15 keV x-rays at the Cornell High Energy Synchrotron Source (CHESS). The instrumental resolution of this measurement is of the same order as the Darwin

<sup>&</sup>lt;sup>24</sup>Element Six, https://www.e6.com/en.



Figure 7: (color online) Rocking curve RMS width topograph taken of the (2,2,0) reflection from a CVD diamond crystal using 15 keV X-rays at the C-line at CHESS. The bright diagonal lines in the corners indicate regions of increased local strain, coinciding with growth boundaries radiating outward from the seed crystal used in the CVD growth process.

width for this diffraction peak, approximately 5  $\mu$ rad. During operation, the 423 electron beam spot would be confined to the relatively uniform central region. 424 Any region in this figure with a rocking curve root-mean-square width of 20  $\mu$ rad 425 or less is indistinguishable from a perfect crystal for the purposes of GLUEX. 426 Regardless of whether or not better HPHT diamonds exist, these Element Six 427 CVD diamonds have sufficiently narrow diffraction widths for our application. 428 This, coupled with their lower cost relative to HPHT material, made them the 429 obvious choice for the Hall-D photon source. 430

The diamond radiator fabrication procedure began with procurement of the 431 raw material in the form of  $7 \times 7 \times 1.2 \text{ mm}^3$  CVD single-crystal plates from 432 the vendor. After x-ray rocking curve scans of the raw material were taken 433 to verify crystal quality, the acceptable diamonds were shipped to a second 434 vendor, Delaware Diamond Knives (DDK). At DDK, the 1.2-mm-thick samples 435 were sliced into three samples of 250  $\mu$ m thickness each, then each one was 436 polished on both sides down to a final thickness close to 50  $\mu$ m. The samples, 437 now of dimensions  $7 \times 7 \times 0.05 \text{ mm}^3$  were fixed to a small aluminum mounting 438 tab using a tiny dot of conductive epoxy placed in one corner. These crystals 439 were then returned to the synchrotron light source for final x-ray rocking curve 440 measurements prior to final approval for use in the GLUEX photon source. 441

The useful lifetime of a diamond radiator in the GLUEX beamline is limited by the degradation in the sharpness of the coherent edge due to accumulation of radiation damage. Experience during the early phase of GLUEX running
showed that after exposure to about 0.5 C of integrated electron beam charge,
the width of the coherent edge increased enough that the entire coherent peak
was no longer contained within the energy window of the tagger microscope.
When a crystal reached this degree of degradation, the radiator was regarded
as no longer usable, and a new crystal was installed.

During Phase 1 of GLUEX, radiator crystals were replaced three times due 450 to degradation, twice with 50  $\mu$ m radiators and once with a 20  $\mu$ m radiator. The 451  $20-\mu m$  diamond was introduced to test whether the reduced multiple Coulomb 452 scattering might result in an observable increase in peak polarization. This 453 turned out not to be the case, for two reasons. The first is that to take full 454 advantage of the reduced multiple scattering in the radiator for increased peak 455 polarization, the collimator size must be reduced proportionally. A 3.4-mm-456 diameter collimator was available for this purpose, but variability observed in 457 the convergence properties of the electron beam at the radiator overruled run-458 ning with any collimator smaller than 5 mm, even when a thinner radiator was 459 in use. 460

The second reason is that any improvements from reduced multiple scat-461 tering that came with the smaller radiator thickness were more than offset by 462 strong indications of radiation damage that appeared not long after the 20  $\mu m$ 463 crystal was put into production. The rapid appearance of radiation damage was 464 partly due to the larger beam current (factor 2.5) that was needed to produce 465 the same photon flux as with a 50  $\mu$ m crystal, but that factor alone did not 466 fully explain what was seen. Subsequent x-ray measurements showed that a 467 large buckling of the 20  $\mu m$  crystal had occurred in the region of the incident 468 electron beam spot, evidently due to local differential expansion of the diamond 469 lattice arising from radiation damage. Once the crystal buckled, the energy 470 of the coherent peak varied significantly across the electron beam spot, effec-471 tively broadening the peak. Fortunately, the greater stiffness of a 50  $\mu$ m crystal 472 appears to suppress this local buckling under similar conditions of radiation 473 damage. 474

Based on these observations, 50  $\mu m$  was selected as the optimum thickness 475 for GLUEX diamond radiators: thin enough to limit the effects of multiple 476 scattering and thick enough to suppress buckling from internal stress induced by 477 radiation damage. The effective useful lifetime of a 50  $\mu$ m radiator in the photon 478 source is about 0.5 C integrated incident electron charge. This lifetime might 479 be extended somewhat by the use of thermal annealing to partially remove the 480 effects of radiation damage. This possibility will be explored when the pace of 481 diamond replacement increases with the start of full-intensity running (GLUEX 482 Phase 2) and the number of spent radiators starts to accumulate. 483

# 484 2.4. Photon tagging system

After passing through the radiator, the combined photon and electron beams enter the photon tagging spectrometer (Tagger). The full-energy electrons are swept out of the beamline by a dipole magnet and redirected into a shielded beam dump. The subset of beam electrons that radiated a significant fraction



Figure 8: Schematic diagram of the tagging spectrometer, showing the paths of the electron and photon beams. Dotted lines indicate post-radiation electron trajectories identified by the energy the electron gave up to an associated radiated photon, as a fraction of the beam energy  $E_0$ . The Tagger focal plane detector arrays TAGH and TAGM are described in the text.

of their energy in the radiator are deflected to larger angles by the dipole field. 489 These post-bremsstrahlung electrons exit through a thin window along the side 490 of the magnet, and are detected in a highly segmented array of scintillators 491 called the Tagger Hodoscope, as shown in Fig.8. The TAGH counters span 492 the full range in energy from 25% to 97% of the full electron beam energy. A 493 high-energy-resolution device known as the Tagger Microscope (TAGM) covers 494 the energy range corresponding to the primary coherent peak, indicated by the 495 denser portion of the focal plane in Fig. 8. The quadrupole magnet upstream of 496 the Tagger dipole provides a weak vertical focus, optimizing the efficiency of the 497 Tagger Microscope for tagging collimated photons. A 0.8 Tm permanent dipole 498 magnet is installed downstream of the Tagger magnet on the photon beam line, 499 in order to prevent the electron beam from reaching Hall D should the Tagger 500 magnet trip. 501

Both the TAGM and TAGH devices are used to determine the energy of 502 individual photons in the photon beam via coincidence, using the relation  $E_{\gamma} =$ 503  $E_0 - E_e$ , where  $E_0$  is the primary electron beam energy before interaction with 504 the radiator, and  $E_e$  is the energy of the post-bremsstrahlung electron deter-505 mined by its detected position at the focal plane. Multiple radiative interactions 506 in a 50  $\mu$ m diamond radiator (3 × 10<sup>-4</sup> radiation lengths) produce uncertainties 507 in  $E_{\gamma}$  of the same order as the intrinsic energy spread of the incident electron 508 beam. 509

# 510 2.4.1. Tagger magnet

The Hall-D Tagger magnet deflects electrons in the horizontal plane, allowing the bremsstrahlung-produced photons to continue to the experimental hall while bending the electrons that produced them into the focal plane detectors. Electrons that lose little or no energy in the radiator are deflected by 13.4° into the electron beam dump.

The Hall-D Tagger magnet is an Elbek-type room temperature dipole magnet, similar to the JLab Hall-B tagger magnet [13, 14]. The magnet is 1.13 m wide, 1.41 m high and 6.3 m long, weighing 80 metric tons, with a normal operating field of 1.5 T for a 12-GeV incident electron beam, a maximum field of
1.75 T, and a pole gap of 30 mm. The magnet design was optimized using the
detailed magnetic field calculation provided by the TOSCA simulation package
and ray tracing of electron beam trajectories [15, 16].

The GLUEX experiment requirements mandate that the scattered electron beam be measured with an accuracy of 12 MeV (0.1% of the incident electron energy). This requires that the magnetic field integrals along all useful electron trajectories be known to 0.1%. The magnetic field was mapped at Jefferson Lab and the detailed field maps were augmented by detailed TOSCA calculations, which have allowed us to meet these goals. Details of the magnet mapping and uniformity are found in Ref. [17].

# 530 2.4.2. Tagger Microscope

The Tagger Microscope (TAGM) is a high-resolution hodoscope that counts 531 post-bremsstrahlung electrons corresponding to the primary coherent peak. Nor-532 mally the TAGM is positioned to cover between 8.2 and 9.2 GeV in photon en-533 ergy, but the TAGM is designed to be movable should a different peak energy be 534 desired. The microscope is segmented along the horizontal axis into 102 energy 535 bins (columns) of approximately equal width. Each column is segmented in five 536 sections (rows) along the vertical axis. The vertical segmentation allows the 537 possibility of scattered electron collimation, which gives a significant increase 538 in photon polarization when used in combination with photon collimation. The 539 purpose of the quadrupole magnet upstream of the dipole is to provide the 540 vertical focus needed to make the double-collimation scheme work efficiently. 541 Summed signals are also available for each column for use in normal operation 542 when electron collimation is not desired. 543

The Tagger Microscope consists of a two-dimensional array of square scin-544 tillating fibers packed in a dense array of dimensions  $102 \times 5$ . The fibers are 545 multi-clad BCF-20 with a  $2 \times 2 \text{ mm}^2$  square transverse profile, manufactured 546 by Saint-Gobain<sup>25</sup>. The cladding varies in thickness from 100 microns near 547 the corners to 70 microns in the middle of the sides, with an active area of 548  $1.8 \times 1.8 \text{ mm}^2$  per fiber. Variations at the level of 5% in the transverse size of 549 the fibers impose a practical lower bound of 2.05 mm on the pitch of the array. 550 The detection efficiency of the TAGM averages 75% across its full energy range, 551 in good agreement with the geometric factor of 77%. 552

Each scintillating fiber is 10 mm long, fused at its downstream end to a clear light guide of matching dimensions (Saint-Gobain BCF-98) that transmits the scintillation light from the focal plane to a shielded box where a silicon photomultiplier (SiPM) converts light pulses into electronic signals. The scintillators are oriented so that the electron trajectories are parallel to the fiber axis, providing large signals for electrons from the radiator, in contrast to the omni-directional electromagnetic background in the tagger hall.

<sup>560</sup> Because the electron trajectories do not cross the focal plane at right angles,

<sup>&</sup>lt;sup>25</sup>Saint-Gobain, https://www.saint-gobain.com/en



Figure 9: Conceptual overview of the tagger microscope design, showing the fiber bundles and light guides (left), and the orientation of these bundles aligned with the incoming electron beam direction in the tagger focal plane (right). The variation of the crossing angle  $\beta$  is exaggerated for the sake of illustration.

the fiber array must be staggered along the dispersion direction. A staggering step occcurs every 6 columns, as illustrated in Fig. 9. The slight variation of the crossing angle  $\beta$  is taken into account by a carefully adjusted fan-out that is implemented by small evenly-distributed gaps at the rear ends of adjacent 6-column groups (bundles). A total of 17 such bundles comprise the full Tagger Microscope.

The far ends of the scintillation light guides are coupled to Hamamatsu 567 S10931-050P SiPMs. The SiPMs are mounted on a custom-built two-stage 568 preamplifier board, with 15 SiPMs per board. In addition to the 15 individual 569 signals generated by each preamplifier, the boards also produce three analog 570 sum outputs, each the sum of five adjacent SiPMs corresponding to the five 571 fibers in a single column. All 510 SiPMs are individually biased by custom bias 572 control boards, one for every two preamplifier boards. The control boards con-573 nect to the preamplifiers over a custom backplane, and communicate with the 574 experimental slow controls system over ethernet. Each control board has the 575 capability to electronically select between two gain modes for the preamplifiers 576 on that board: a low gain mode used during regular tagging operation, and a 577 high gain mode used for triggering on single-pixel pulses during bias calibration. 578 Each bias control board manages the control and biasing for two preamplifiers. 579 The control board also measures live values for environmental parameters (volt-580 age levels and temperatures) in the TAGM electronics, so that alarms can be 581 generated by the experimental control system whenever any of these parameters 582 stray outside predefined limits. 583

Pulse height and timing information for 122 channels from the TAGM is provided by analog-to-digital converters (ADCs) and time-to-digital converters (TDCs). These 122 signals include the 102 column sums plus the individual fiber signals from columns 7, 27, 81, and 97. Here, each channel goes through a 1:1 passive splitter, with one output going to an ADC and the other through discriminators to a TDC. The ADCs are 250-MHz flash ADCs with 12-bit resolution and a full-scale pulse amplitude of 1 V. The TDCs are based on the F1 TDC chip [18], with a least-count of 62 ps. Pulse thresholds in both the ADC and discriminator modules are programmable over the range 1-1000 mV on an individual channel basis, covering the full dynamic range of the TAGM front end. The TAGM preamplifier outputs (before splitting) saturate at around 2 V pulse amplitude.

The mean pulse charge in units of SiPM pixels corresponding to a single 596 high-energy electron varies from 150 to 300 pC, depending on the fiber, with 597 an average of 220 pC and standard deviation of 25 pC. During calibration, this 598 yield is measured individually for each fiber by selectively biasing the SiPMs on 599 each row of fibers, one row at a time, and reading out the column sums. Once 600 all 510 individual fiber yields have been measured, the bias voltages within each 601 column are adjusted to compensate for yield variations, so that the mean pulse 602 height in a given column is the same regardless of which fiber in the column 603 detected the electron. The ADC readout and discriminator thresholds are set 604 individually for each column, for optimum efficiency and noise rejection. 605

The ADC firmware provides an approximate time for each pulse, in addition 606 to the pulse amplitude. During offline reconstruction, this time information 607 is used to associate ADC and TDC pulse information from the same channel, 608 so that a time-walk correction can be applied to the TDC time. Once this 609 correction has been applied, a time resolution of 230 ps is achieved for the 610 TAGM. This resolution is based on data collected at rates on the order of 1 MHz 611 per column, while the typical rate in the tagger microscope is about 0.5 MHz. 612 The readout was designed to operate at rates up to 4 MHz per column. A brief 613 test above 2 MHz per column allowed visual inspection of the pulse waveforms 614 from the TAGM, without change in the pulse shape or amplitude. 615

## 616 2.4.3. Broadband tagging hodoscope

The Tagger Hodoscope (TAGH) consists of 222 scintillator counters dis-617 tributed over a length of 9.25 m and mounted just behind the focal plane of 618 the tagger magnet. The function of this hodoscope is to tag the full range of 619 photon energy from 25% to 97% of the incident electron energy. A gap in the 620 middle of that range is left open for the registration of the primary coherent 621 peak by the Tagger Microscope. The geometry of the counters in the vicinity 622 of the microscope is shown in Fig. 10. This broad coverage aids in alignment of 623 the diamond radiator and expands the GLUEX physics program reach to photon 624 energies outside the range of the coherent peak. The coverage of the hodoscope 625 counters in the region below 60% drops to half, with substantial gaps in energy 626 between the counters. This was done because the events of primary interest to 627 GLUEX come from interactions of photons within and above the coherent peak; within and above the coherent peak the coverage is 100% up to the 97%  $E_0$ 629 cutoff. 630

Each counter in the hodoscope is a sheet of EJ-228 scintillator, 6 mm thick and 40 mm high. The counter widths vary along the focal plane, from 21 mm



Figure 10: Schematic of electron trajectories in the region of the microscope. Shown are the three layers of hodoscope counters on either side of the microscope and the region covered by the microscope.

<sup>633</sup> near the end-point region down to 3 mm at the downstream end. The scintil-<sup>634</sup> lators are coupled to a Hamamatsu R9800 photomultiplier tube (PMT) via a <sup>635</sup> cylindrical acrylic (UVT-PMMA) light guide 22.2 mm in diameter and 120 mm <sup>636</sup> long. Each PMT is wrapped in  $\mu$ -metal to shield the tube from the fringe field <sup>637</sup> of the tagger magnet.

Each PMT is instrumented with a custom designed active base [19], con-638 sisting of a high-voltage divider and an amplifier powered by current flowing 639 through the divider. The base provides two signal outputs, one going to a flash 640 ADC and the other through a discriminator to a TDC. Operating the amplifier 641 with a gain factor of 8.5 allows the PMT to operate at a lower voltage of 900 V 642 and reduce the PMT anode current, therefore improving the rate capability. 643 The energy bite of each counter ranges between 8.5 and 30 MeV for a 12 GeV 644 incident electron beam. Typical rates during production running are 1 MHz 645 above the coherent peak and 2 MHz per counter below the coherent peak. The 646 maximum sustainable rate per counter is about 4 MHz. 647

The counters are mounted with their faces normal to the path of the scattered electrons in two or three rows slightly downstream of the focal plane, as shown in Fig. 10. This allows the counters to be positioned without horizontal gaps in the dispersion direction, enabling complete coverage of the entire tagged photon energy range.

The mounting frame of the hodoscope is suspended from the ceiling of the Tagger Hall to provide full flexibility for positioning TAGH. The frame is constructed to also support the addition of counters to fill in the energy range currently occupied by the microscope when the TAGM location is changed.

A similar procedure to that described in Section 2.4.2 for the TAGM is used 657 to apply a time-walk correction to the TDC times from the TAGH counters. 658 Once this time-walk correction is applied, the time resolution of the TAGH is 659 200 ps. No significant degradation of this resolution is expected at the operating 660 rates planned for Phase 2 running, which are on the order of 2 MHz per counter 661 above the coherent peak. Under these conditions, the rates in the TAGH coun-662 ters below the coherent peak would average around 4 Mhz, which is at the top 663 of their allowed range. These counters will be turned off when running at full 664



Figure 11: Attenuation of low-energy photons in foils with a thickness of 3% of a radiation length for different materials as a function of photon energy. The W foil was selected to reduce the random background hits in the detector drift chambers. The attenuation coefficients are taken from Ref. [20].

## 665 intensity.

## 666 2.5. Tungsten keV filter

To reduce the photon flux in the 10 - 100 keV range, a 100  $\mu$ m tungsten 667 foil (3% of a radiation length) was installed in the beam line at the entrance of 668 the collimator cave. We have studied the effect of different foil materials on the 669 anode currents and random hits in the drift chambers (see Section 5), as these 670 factors limit the high-intensity operation of the experiment. By comparing the 671 effect of different materials (Al, Cu, W) with fixed radiation lengths (see Fig.11) 672 we learned that the drift chambers are mostly affected by photons in the 70-90 673 keV range. The analysis of the pulse shape of the random hits in the CDC 674 confirmed that these photons directly produce hits in the inner layers of the 675 chamber. The insertion of the tungsten foil reduced the number of random hits 676 in the inner CDC layers by a factor of up to 8 and the anode current by 55%. 677 The reduction of the current in the FDC was more moderate, about 25%. Note 678 that the FDC sense wires are as close as 3 cm to the beam, while in the CDC 679 the closest wires are at 10 cm. 680

#### 681 2.6. Beam profiler

The beam profiler is located immediately upstream of the collimator (see Fig. 4) and is used to measure the photon beam intensity in a plane normal to the incident photon beam. The profiler consists of two planes of scintillating fibers, giving information on the photon beam profile in the X and Y projections. Each plane consists of 64 square fibers, 2 mm in width, read out by four 16channel multi-anode PMTs. The beam profiler is only used during beam setup until the photon beam is centered on the active collimator.

#### 689 2.7. Active collimator

The active collimator monitors the photon beam position and provides feed-690 back to micro-steering magnets in the electron beamline, for the purpose of 691 suppressing drifts in photon beam position. The design of the active collimator 692 for GLUEX is based on a device developed at SLAC for monitoring the coherent 693 bremsstrahlung beam there [21]. The GLUEX active collimator is located on 694 the upstream face of the primary collimator, and consists of a dense array of 695 tungsten pins attached to tungsten base plates. The tungsten plate intercepts 696 off-axis beam photons before they enter the collimator, creating an electromag-697 netic shower that cascades through the array of pins. High-energy delta rays 698 created by the shower in the pins (known as "knock-ons") are emitted forward 699 into the primary collimator. The resulting net current between the tungsten 700 plates and the collimator is proportional to the intensity of the photon beam on 701 the plate. The tungsten plates are mounted on an insulating support, and the 702 plate currents are monitored by a preamplifier with pA sensitivity. 703

The tungsten plate is segmented radially into two rings, and each ring is 704 segmented azimuthally into four quadrants. The asymmetry of the induced 705 currents on the plates in opposite quadrants indicates the degree of displace-706 ment of the photon beam from the intended center position. Typical currents 707 on the tungsten sectors are at the level of 1.4 nA (inner ring) and 0.85 nA 708 (outer ring) when running with a 50  $\mu$ m diamond crystal and a 200-nA incident 709 electron beam current. The current-sensitive preamplifiers used with the ac-710 tive collimator are PMT-5R devices manufactured by ARI Corporation<sup>26</sup>. The 711 PMT-5R has six remotely selectable gain settings ranging from  $10^{12}$  V/A to 712  $10^6$  V/A, selectable by powers of 10. This provides an excellent dynamic range 713 for operation of the beam over a wide range of intensities, from 1 nA up to sev-714 eral  $\mu$ A. The preamplifier input stage exhibits a fixed gain-bandwidth product 715 of about 2 Hz-V/pA which limits its bandwidth at the higher gain settings, for 716 example 2 Hz at  $10^{12}$  V/A, 20 Hz at  $10^{11}$  V/A. 717

In-situ electronic noise on the individual wedge currents is measured to be 718 1.5 pA/ $\sqrt{\text{Hz}}$  on the inner ring, and 15 pA/ $\sqrt{\text{Hz}}$  on the outer ring. The sensi-719 tivity of the current asymmetry to position is 0.160/mm for the inner ring and 720 0.089/mm for the outer. With a 50 micron diamond and 200 nA beam current, 721 operating the active collimator at a bandwidth of 1 kHz yields a measurement 722 error in the position of the beam centroid of 150  $\mu$ m for the inner ring and 723 450  $\mu$ m for the outer ring. The purpose of the outer ring is to help locate the 724 beam when the beam location has shifted more than 2 mm from the collimator 725 axis, where the response of the inner ring sectors becomes nonlinear. 726

The maximum deviation allowed for the Hall D photon beam position relative to the collimator axis is 200  $\mu$ m. The active collimator readout was designed with kHz bandwidth so that use in a fast feedback loop would suppress motion of the beam at 60 Hz and harmonics that might exceed this limit. Experience with the Hall-D beam has shown that the electron beam feedback system already

<sup>&</sup>lt;sup>26</sup>Advanced Research Instruments Corporation, http://aricorp.com.

suppresses this motion to less than 100  $\mu$ m amplitude, so that fast feedback us-732 ing the active collimator is not required during normal operation. Instead, the 733 active collimator is used in a slow feedback loop which locks the photon beam 734 position at the collimator with a correction time constant of a few seconds. This 735 slow feedback system is essential for preventing long-term drifts in the photon 736 beam position that would otherwise occur on the time scale of hours or days. 737 The active collimator can achieve 200  $\mu$ m position resolution down to beam 738 currents as low as 2 nA when operated in this mode with noise averaging over 739 a 5 s interval. 740

#### 741 2.8. Collimator

The photon beam produced at the diamond radiator contains both inco-742 herent and coherent bremsstrahlung components. In the region of the coherent 743 peak, where photon polarization is at its maximum, the angular spread of coher-744 ent bremsstrahlung photons is less than that of incoherent bremsstrahlung. The 745 characteristic emission angle for incoherent bremsstrahlung is  $m/E = 43 \ \mu rad$ 746 at 12 GeV, whereas the coherent flux within the primary peak is concentrated 747 below 15  $\mu$ rad with respect to the beam direction. Collimation increases the 748 degree of linear polarization in the photon beam by suppressing the incoherent 749 component relative to the coherent part. 750

The Hall-D primary collimator provides apertures of 3.4 mm and 5.0 mm in a 751 tungsten block mounted on an X-Y table. The 5.0 mm collimator is used under 752 normal GLUEX running conditions. The tungsten collimator is surrounded by 753 lead shielding. The collimator may also be positioned to block the beam to 754 prevent high-intensity beam from entering the experimental hall during tuning 755 of the electron beam. Downstream of the primary collimator, a sweeping magnet 756 and shield wall, followed by a secondary collimator with its sweeping magnet 757 and shield wall, suppress charged particles and photon background around the 758 photon beam that are generated in the primary collimator. The photon beam 759 exiting the collimation system then passes through a thin pair conversion target. 760 The resulting  $e^+e^-$  pairs are used to continuously monitor the photon beam flux 761 and polarization. 762

#### 763 2.9. Triplet Polarimeter

The Triplet Polarimeter (TPOL) is used to measure the degree of polarization of the linearly-polarized photon beam [22]. The polarimeter uses the process of  $e^+e^-$  pair production on atomic electrons in a beryllium target foil, with the scattered atomic electrons measured using a silicon strip detector. Information on the degree of polarization of the photon beam is obtained by analyzing the azimuthal distribution of the scattered atomic electrons.

#### 770 2.9.1. Determination of photon polarization

Triplet photoproduction occurs when the polarized photon beam interacts with the electric field of an atomic electron within a target material and produces a high energy  $e^+e^-$  pair. When coupled with trajectory and energy

information of the  $e^+e^-$  pair, the azimuthal angular distribution of the recoil 774 electron provides a measure of the photon beam polarization. The cross sec-775 tion for triplet photoproduction can be written as  $\sigma_t = \sigma_0 [1 - P\Sigma \cos(2\varphi)]$  for 776 a polarized photon beam, where  $\sigma_0$  is the unpolarized triplet cross section, P 777 the photon beam polarization,  $\Sigma$  the beam asymmetry for the process, and  $\varphi$ 778 the azimuthal angle of the recoil electron trajectory with respect to the plane 779 of polarization for the incident photon beam. To determine the photon beam 780 polarization, the azimuthal distribution of the recoil electrons is recorded and 781 fit to the function  $A[1-B\cos(2\varphi)]$  where the variables A and B are parameters 782 of the fit, with  $B = P\Sigma$ . The value of  $\Sigma$  depends on the beam photon energy, 783 the thickness of the converter target, and the geometry of the setup. The value 784 of  $\Sigma$  was determined to be  $0.1990 \pm 0.0008$  at 9 GeV for the GLUEX beamline 785 and a 75 micron Be converter [22]. 786

The TPOL detects the recoil electron arising from triplet photoproduction. 787 This system consists of a converter tray and positioning assembly, which holds 788 and positions a beryllium foil converter where the triplet photoproduction takes 789 place. A silicon strip detector (SSD) detects the recoil electron from triplet 790 photoproduction, providing energy and azimuthal angle information for that 791 particle. A vacuum housing, containing the pair production target and SSD, 792 supplies a vacuum environment minimizing multiple Coulomb scattering be-793 tween target and SSD. Preamplier and signal filtering electronics are placed 794 within a Faraday-cage housing. 795

The preamplifier enclosure is lined with a layer of copper foil to reduce exterior electromagnetic signal interference. Signals from the downstream (azimuthal sector) side of the SSD are fed to a charge-sensitive preamplifier located outside the vacuum. In operation, the TPOL vacuum box is coupled directly to the evacuated beamline through which the polarized photon beam passes.

Upon entering TPOL, the photon beam passes into the beryllium converter, 801 triplet photoproduction takes place, an  $e^+e^-$  pair is emitted from the target 802 in the forward direction, and a recoil electron ejected from the target at large 803 angles with respect to the beam is detected by the SSD within the TPOL vacuum 804 chamber. The recoil electron is ejected at large angles and detected by the SSD. 805 The  $e^+e^-$  pair, together with any beam photons that did not interact with the 806 converter material, pass through the downstream port of the TPOL vacuum 807 box into the evacuated beamline, which in turn passes through a shielding wall 808 into the Hall-D experimental area. The  $e^+e^-$  pair then enters the vacuum box 809 and magnetic field of the GLUEX Pair Spectrometer, while photons continue 810 through an evacuated beamline to the target region of the GLUEX detector. 811 Accounting for all sources of uncertainty from this setup, the total estimated 812 systematic error in the TPOL asymmetry  $\Sigma$  is 1.5% [22]. 813

#### 814 2.10. Pair Spectrometer

The main purpose of the Pair Spectrometer (PS) [23] is to measure the spectrum of the collimated photon beam and determine the fraction of linearly polarized photons in the coherent peak energy region. The TPOL relies on the PS to trigger on pairs in coincidence with hits in the recoil detector. The PS is also used to monitor the photon beam flux, and for energy calibration of the
 tagging hodoscope and microscope detectors.

The PS, located at the entrance to Hall D, reconstructs the energy of a 821 beam photon by detecting the  $e^+e^-$  pair produced by the photon in a thin 822 converter. The converter used is typically the beryllium target housed within 823 TPOL; otherwise the PS has additional converters that may be inserted into the 824 beam with thicknesses ranging between 0.03% and 0.5% of a radiation length. 825 The produced  $e^+e^-$  leptons are deflected in a modified 18D36 dipole magnet 826 with an effective field length of about 0.94 m and detected in two layers of 827 scintillator detectors: a high-granularity hodoscope and a set of coarse counters, 828 referred to as PS and PSC counters, respectively. The detectors are partitioned 829 into two identical arms positioned symmetrically on opposite sides of the photon 830 beam line. The PSC consists of sixteen scintillator counters, eight in each 831 detector arm. Each PSC counter is 4.4 cm wide and 2 cm thick in the direction 832 along the lepton trajectory and 6 cm high. Light from the PSC counters is 833 detected using Hamamatsu R6427-01 PMTs. The PS hodoscope consists of 145 834 rectangular tiles (1 mm and 2 mm wide) stacked together. Hamamatsu SiPMs 835 were chosen for readout of the PS counters [24, 25, 26]. 836

Each detector arm covers an  $e^{\pm}$  momentum range between 3.0 GeV/c and 6.2 GeV/c, corresponding to reconstructed photon energies between 6 GeV and 12.4 GeV. The relatively large acceptance of the hodoscope enables energy determination for photons with energies from below the coherent peak to the beam endpoint energy near 12 GeV.

The pair energy resolution of the PS hodoscope is about 25 MeV. The time resolution of the PSC counters is 120 ps, which allows coincidence measurements between the tagging detectors and the PS within an electron beam bunch. Signals from the PS detector are delivered to the trigger system, as described in Section 9. The typical rate of PS double-arm coincidences is a few kHz. Details about the performance of the spectrometer are given in [27, 28].

# 848 2.10.1. Determination of photon flux

The intensity of beam photons incident on the GLUEX target is important for 849 the extraction of cross sections. The photon flux is determined by converting a 850 known fraction of the photon beam to  $e^{\pm}$  pairs and counting them in the PS as a 851 function of energy. Data from the PS are collected using a PS trigger, which runs 852 in parallel to the main GLUEX physics trigger, as described in Section 9. The 853 number of beam photons integrated over the run period is obtained individually 854 for each tagger counter (TAGH and TAGM), i.e., for each photon beam energy 855 bin. 856

The PS calibration parameter used in the flux determination, a product of the converter thickness, acceptance, and the detection efficiency for leptons, is determined using calibration runs with the Total Absorption Counter (TAC) [29]. The TAC is a small calorimeter (see Section 2.11) inserted directly into the photon beam immediately upstream of the photon beam dump to count the number of beam photons as a function of energy. These absolute-flux calibration runs are performed at reduced beam intensities in order to limit the rate of accidental tagging coincidences. Data are acquired simultaneously from the PS and TAC. These data enable an absolute flux calibration for the PS by measuring the number of reconstructed  $e^+e^-$  pairs for a given number of photons of the same energy seen by the TAC. Uncertainties on the photon flux determinations are currently being investigated. The expected precision of the flux determination is on the level of 1%.

#### 870 2.11. Total Absorption Counter

The TAC is a high-efficiency lead-glass calorimeter, used at low beam cur-871 rents (< 5nA) to determine the overall normalization of the flux from the GLUEX 872 coherent bremsstrahlung facility. This device is intended to count all beam pho-873 tons above a certain energy threshold, which have a matching hit in the tagger 874 system. There would be a very large number of overlapping pulses in the TAC 875 if it is used with the production photon flux, resulting in low detection effi-876 ciency and therefore large systematic uncertainties. Therefore, the TAC is only 877 inserted into the beam during dedicated runs at very low intensities when the 878 detector can run with near 100% efficiency. The TAC was originally developed 879 for and deployed in Hall B, for photon beam operations with CLAS [30, 31, 32]. 880 Only a certain fraction of the photons produced at the radiator reach the 881 target and causes an interaction that is seen in the GLUEX detector. The 882

count of tagged photons reaching the GLUEX target is determined as a function 883 of energy from individual TAC coincidence measurements with each tagging 884 counter. Simultaneous with these counts, the coincidences between each of the 885 tagging counters and converted pairs detected in the pair spectrometer are also 886 recorded. The ratio between the count of tagged pairs and tagged TAC events 887 thus determined for each tagging counter are used to convert the tagged rate 888 in the pair spectrometer that is observed during normal operation into a total 889 count of tagged photons for each tagging counter that were incident on the 890 GLUEX target. 891

## <sup>892</sup> 3. Solenoid magnet

## 893 3.1. Overview

The core of the GLUEX spectrometer is a superconducting solenoid with a bore diameter and overall yoke length of approximately 2 m and 4.8 m, respectively. The photon beam passes along the axis of the solenoid. At the nominal current of 1350 A, the magnet provides a magnetic field along the axis of about 2 T.

The magnet was designed and built at SLAC in the early 1970's [33] for the LASS spectrometer [34]. The solenoid employs a cryostatically stable design with cryostats designed to be opened and serviced with hand tools. The magnet was refurbished and modified<sup>27</sup> for the GLUEX experiment [35, 36].

 $<sup>^{27}</sup>$  The front plate of the flux return yoke was modified, leading to a swap of the two front

The magnet is constructed of four separate superconducting coils and cryostats. The flux return yoke is made of several iron rings. The coils are connected in series. A common liquid helium tank is located on top of the magnet, providing a gravity feed of the liquid to the coils. The layout of the coil cryostats and the flux return iron yoke is shown in Fig. 3. Table 3 summarizes the salient parameters of the magnet.

Inside diameter of coils	$2032~\mathrm{mm}$
Clear bore diameter	$1854~\mathrm{mm}$
Overall length along iron	4795  mm
Inside iron diameter	$2946~\mathrm{mm}$
Outside iron diameter	$3759 \mathrm{~mm}$
Original yoke, cast and annealed - steel	AISI 1010
Added filler plates - steel	ASTM A36
Full weight	284 t
Full number of turns	4608
Number of separate coils	4
Turns per coil 2	928
Turns per coil 1	1428
Turns per coil 3	776
Turns per coil 4	1476
Total conductor weight	13.15 t
Coil resistance at $\sim 300$ K	$15.3 \ \Omega$
Coil resistance at $\sim 10$ K	${\sim}0.15~\Omega$
Design operational current	1500 A
Nominal current (actual)	1350 A
Maximal central field at 1350 A	$2.08 \mathrm{~T}$
Inductance at 1350 A	$26.4~\mathrm{H}$
Stored energy at 1350 A	$24.1 \ \mathrm{MJ}$
Protection circuit resistor	$0.061~\Omega$
Coil cooling scheme	helium bath
Total liquid helium volume	$3200~\ell$
Operating temperature (actual)	$4.5~\mathrm{K}$
Refrigerator liquefaction rate at 0 A	$1.7 \mathrm{~g/s}$
Refrigerator lique faction rate at 1350 ${\rm A}$	$2.7 \mathrm{~g/s}$

Table 3: Key parameters of the GLUEX solenoid. The coils are listed in order along the beam direction.

#### 909 3.2. Conductor and Coils

The superconductor composite is made of niobium-titanium filaments in a copper substrate, twisted and shaped into a  $\sim 7.62 \times 1 \text{ mm}^2$  rectangular band.

coils and modifications of the return flux yoke in order to keep the magnetic forces on the front coil under the design limit. The original gaps between the yoke's rings were filled with iron. The Cryogenic Distribution Box was designed and built for GLUEX.

The laminated conductor is made by soldering the superconductor composite band between two copper strips to form a rectangular cross section of  $7.62 \times 5.33 \text{ mm}^2$ . The measured residual resistivity ratio of the conductor at  $\sim 300 \text{K}$  and  $\sim 15 \text{K}$  is  $\approx 100$ .

As the coil was wound, a 0.64 mm-thick stainless steel support band and two 0.2 mm-thick Mylar insulating strips were wound together with it for pretensioning and insulation. The liquid helium is in contact with the shorter (5.33 mm) sides of the cable.

Each of the coils consists of a number of subcoils. Each subcoil contains a number of "double pancakes" with the same number of turns. Each double pancake is made from a single piece of conductor. The voltage across the subcoils is monitored using special wires. These pass through vertical cryostats, called chimneys, along with the helium supply pipes and the main conductor.

The cold helium vessel containing the coil is supported within the warm cryostat vacuum vessel by a set of columns designed to provide sufficient thermal insulation. The columns are equipped with strain gauges for monitoring the stresses on the columns. The helium vessel is surrounded by a nitrogen-cooled thermal shield made of copper and stainless-steel panels. Super-insulation is placed between the vacuum vessel and the nitrogen shield. The vacuum vessels are attached to the matching iron rings of the yoke.

The power supply<sup>28</sup> provides up to 10 V DC for establishing the operating 932 current while ramping. The supply also includes a protection circuit, which 933 can be engaged by a quench detector as well as by other signals. During trips, 934 a small dump resistor of 0.061  $\Omega$  limits the maximum voltage on the magnet 935 to 100 V. The dumping time constant of  $L/R \approx 7$  min is relatively long, but 936 safe according to the original design of the magnet. A large copper mass and 937 the helium bath are able to absorb a large amount of energy during a quench 938 without overheating the solder joints. This permits the use of an "intelligent" 939 quench detector with low noise sensitivity and a relatively slow decision time 940 of 0.5 s. The quench detector compares the measured voltages on different 941 subcoils in order to detect a resistive component. While ramping the current, 942 such a voltage is proportional to the subcoil inductance. Relative values of 943 inductance of various subcoils depend on the value of the current because of 944 saturation effects in the iron yoke. Transient effects are also present at changes 945 of the slew rate caused by Foucault currents in the yoke. The system includes 946 two redundant detectors: one uses analog signals and a simplified logic, another 947 is part of the PLC control system (see Section 3.4) which uses digitized signals. 948 The PLC digital programmable device is more sensitive since this monitoring 949 system takes into account the dependence of the coils' inductance on the current 950 and provides better noise filtering. The ramping slew rate is limited by the 951 transient imbalance of the voltages on subcoils that may trigger the quench 952 detector. Additionally, unexplained voltage spikes of 1 ms duration have been 953 observed in coil 2 at high slew rates, which can trigger the quench detector. 954

<sup>&</sup>lt;sup>28</sup>Danfysik System 8000 Type 854.

Powering up the magnet to 1350 A takes about 8 h.

For diagnostic purposes two 40-turn pickup coils are installed on the bore surface of the vacuum vessel of each of the coils.

## 958 3.3. Cooling System

The cooling system is described in detail in Ref. [37]. A stand-alone helium 959 refrigerator located in a building adjacent to Hall D provides liquid helium and 960 nitrogen via a transfer line to the Cryogenic Distribution Box above the magnet. 961 The transfer line delivers helium at 2.6 atm, and 6 K to a Joule-Thomson (JT) 962 valve providing liquid to a cylindrical common helium tank in the Distribution 963 Box. The level of liquid helium in the tank is measured with a superconducting 964 wire probe;<sup>29</sup> the liquid level is kept at about half of the tank diameter. The 965 cold helium gas from the tank is returned to the refrigerator, which keeps the 966 pressure at the top of the tank at 1.2 atm corresponding to about 4.35 K at 967 the surface of the liquid.<sup>30</sup> Each coil is connected to the common helium tank 968 by two vertical 2-inch pipes. One pipe is open at the bottom of the tank while 969 the other one is taller than the typical level of helium inside the tank. The 970 main conductor and the wires for voltage monitoring pass through the former 971 pipe. Additionally, two  $\sim 6$  m long, 3/8 inch ID pipes go outside the coil's 972 helium vessel, from the Distribution Box to the bottom of the coil. One of those 973 pipes, connected to a JT valve in the box, is used to fill the coil initially, but is 974 not used during operation. The other pipe reaches the bottom of the common 975 helium tank in order to provide a thermo-syphon effect essential for the proper 976 circulation of helium in the coil. The main current is delivered into the helium 977 tank via vapor-cooled leads, and is distributed to the coils by a superconducting 978 cable. After cooling the leads, the helium gas is warmed and returned to the 979 refrigeration system. The gas flow through the leads is regulated based on the 980 current in the magnet; at 1350 A, the flow is about 0.25 g/s. The coils and the 981 Distribution Box are equipped with various sensors for temperature, pressure, 982 voltage, and flow rates. 983

#### 984 3.4. Measurements and Controls

The control system for the superconducting solenoid, power supply, and cryogenic system, is based on Programmable Logic Controllers (PLC)<sup>31</sup>. The PLC system digitizes the signals from various sensors, communicates with other devices, reads out the data into a programmable unit for analysis, and sends commands to various devices. Additionally, the PLC is connected to EPICS<sup>32</sup> in order to display and archive the data (see Section 11). The practical sampling limit for the readout of the sensor is a few Hz, which is too low for detection of

<sup>&</sup>lt;sup>29</sup> American Magnetics Model 1700 with HS-1/4-RGD-19"/46"-4LDCP-LL6-S sensor

<sup>&</sup>lt;sup>30</sup> The original implementation at SLAC did not recycle the helium and operated at atmospheric pressure.

<sup>&</sup>lt;sup>31</sup> Allen-Bradley Programmable Logic Controllers http://ab.rockwellautomation.com/ Programmable-Controllers.

<sup>&</sup>lt;sup>32</sup>Experimental Physics and Industrial Control System, https://epics.anl.gov.

fast voltage spikes on the coils due to motion, shorts, or other effects. Therefore, 992 the voltage taps from the coils and the pickup coils are read out by a PXI 993 system<sup>33</sup>, which provides a sampling rate of about 100 kHz. The PXI system 994 also reads out several accelerometers attached to the coils' chimneys, which can 995 detect motion inside the coils. The PXI CPU performs initial integration and 996 arranges the data in time-wise rows with a sampling rate of 10 kHz. The PLC 997 system reads out the data from the PXI system. Additionally, the PXI data are 998 read out by an EPICS server at the full 10 kHz sampling rate and are recorded 999 for further analysis. 1000

#### 1001 3.5. Field calculation and measurement

The momentum resolution of the GLUEX spectrometer is larger than 1%1002 and is dominated by multiple scattering and the spatial resolution of the coor-1003 dinate detectors. Thus, a fraction of a percent is sufficient accuracy for the field 1004 determination. The coils are axially symmetric, while the flux return yoke is 1005 nearly axially symmetric, apart from the holes for the chimneys. The field was 1006 calculated using a 2-dimensional field calculator Poisson/Superfish<sup>34</sup>, assuming 1007 axial symmetry. The model of the magnet included the fine structure of the 1008 subcoils and the geometry of the voke iron. Different assumptions about the 1009 magnetic properties of the yoke iron have been used: the *Poisson* default AISI 1010 1010 steel, the measurements of the original voke iron made at SLAC, and the 1011 1018 steel used for the filler plates. Since the results of the field calculations 1012 differ by less than 0.1%, the default *Poisson* AISI 1010 steel properties were 1013 used for the whole yoke iron in the final field map calculations. 1014

The three projections of the magnetic field have been measured along lines 1015 parallel to the axis, at four values of the radius and at up to six values of 1016 the azimuthal angle. The calculated field and the measured deviations are 1017 shown in Fig. 12. The tracking detectors occupy the volume of R < 56 cm 1018 and 45 < Z < 340 cm. In this volume the field deviation at R = 0 does not 1019 exceed 0.2%. The largest deviation of 1.5% is observed at the downstream edge 1020 of the fiducial volume and at the largest radius. Such a field uncertainty in 1021 that region does not noticeably affect the momentum resolution. In most of the 1022 fiducial volume the measured field is axially symmetric to  $\approx 0.1\%$  and deviates 1023 from this symmetry by  $\approx 2\%$  at the downstream edge and the largest radius. 1024

<sup>1025</sup> The calculated field map is used for track reconstruction and physics analy-<sup>1026</sup> ses.

# 1027 4. Target

<sup>1028</sup> A schematic diagram of the GLUEX liquid hydrogen cryotarget is shown in <sup>1029</sup> Fig. 13. The major components of the system are a pulse tube cryocooler,<sup>35</sup>

codes.phtml#ps.

<sup>&</sup>lt;sup>33</sup> National Instruments, PXI Platform, http://www.ni.com/pxi/.

<sup>&</sup>lt;sup>34</sup> Poisson/Superfish developed at LANL, https://laacg.lanl.gov/laacg/services/serv\_

<sup>&</sup>lt;sup>35</sup>Cryomech model PT415.



Figure 12: The full field at 1350 A calculated with *Poisson* (left scale) on the axis and at the edge of the tracking fiducial volume (R=56 cm). The deviations of the measurements from the calculations are shown (right scale) on the axis, and at R=56 cm. The measurements were made at 6 azimuthal angles. We show the angles  $(0^{\circ} \text{ and } 90^{\circ})$  with the largest deviations from the calculations.

a condenser, and a target cell. These items are contained within an aluminum 1030 and stainless steel 'L'-shaped vacuum chamber with an extension of closed-cell 1031 foam<sup>36</sup> surrounding the target cell. In turn, the GLUEX Start Counter (Sec. 8.1) 1032 surrounds the foam chamber and is supported by the horizontal portion of the 1033 vacuum chamber. Polyimide foils, 100  $\mu$ m thick, are used at the upstream and 1034 downstream ends of the chamber as beam entrance and exit windows. The 1035 entire system, including the control electronics, vacuum pumps, gas-handling 1036 system, and tanks for hydrogen storage, is mounted on a small cart that is 1037 attached to a set of rails for insertion into the GLUEX solenoid. To satisfy 1038 flammable gas safety requirements, the system is connected at multiple points 1039 to a nitrogen-purged ventilation pipe that extends outside Hall D. 1040

<sup>1041</sup> Hydrogen gas is stored inside two 200 l tanks and is cooled and condensed <sup>1042</sup> into a small copper and stainless steel container, the condenser, that is thermally <sup>1043</sup> anchored to the second cooling stage of the cryocooler. The first stage of the <sup>1044</sup> cryocooler is used to cool the H<sub>2</sub> gas to about 50 K before it enters the condenser. <sup>1045</sup> The first stage also cools a copper thermal shield that surrounds all lower-<sup>1046</sup> temperature components of the system except for the target cell itself, which is <sup>1047</sup> wrapped in a few layers of aluminized-mylar/cerex insulation.

<sup>&</sup>lt;sup>36</sup>Rohacell 110XT, Evonik Industries AG.



Figure 13: Simplified process and instrumentation diagram for the GlueX liquid hydrogen target (not to scale). In the real system, the P-trap is above the level of the target cell and is used to promote convective cooling of the target cell from room temperature.

The condenser is comprised of a copper C101 base sealed to a stainless steel can with an indium O-ring. Numerous vertical fins are cut into the copper base, giving a large surface area for condensing hydrogen gas. A heater and a pair of calibrated Cernox thermometers<sup>37</sup> are attached outside the condenser, and are used to regulate the heater temperature when the system is filled with liquid hydrogen.

The target cell, shown in Fig. 14, is similar to designs used in Hall B at 1054 JLab [38]. The cell walls are made from 100- $\mu$ m-thick aluminized polyimide 1055 sheet wrapped in a conical shape and glued along the edge, overlapping into 1056 a 2 mm wide scarf joint. The conical shape prevents bubbles from collecting 1057 inside the cell, while the scarf joint reduces the stress riser at the glue joint. 1058 This conical tube is glued to an aluminum base, along with stainless steel fill 1059 and return tubes leading to the condenser, a feed-through for two calibrated 1060 Cernox thermometers inside the cell, and a polyamide-imide support for the 1061 reentrant upstream beam window. Both the upstream and downstream beam 1062 windows are made of non-aluminized, 100  $\mu$ m thick polyimide films that have 1063 been extruded into the shapes indicated in Fig. 14. These windows are clearly 1064 visible in Fig. 21 where reconstructed vertex positions are shown. All items are 1065 glued together using a two-part epoxy<sup>38</sup> that has been in reliable use at cryogenic 1066

<sup>&</sup>lt;sup>37</sup>Cernox, Lake Shore Cryotronics.

 $<sup>^{38}3\</sup>mathrm{M}$  Scotch-Weld epoxy adhesive DP190 Gray.



Figure 14: Target cell for the liquid hydrogen target. Dimensions are in mm.

temperatures for long periods. A second heater, attached to the aluminum base, is used to empty the cell for background measurements. The base is attached to a kinematic mount, which is in turn supported inside the vacuum chamber using a system of carbon fiber rods. The mount is used to correct the pitch and yaw of the cell, while X, Y, and Z adjustments are accomplished using positioning screws on the target cart.

During normal operation, a sufficient amount of hydrogen gas is condensed 1073 from the storage tanks until the target cell, condenser, and interconnecting 1074 piping are filled with liquid hydrogen and an equilibrium pressure of about 1075 19 psia is achieved. The condenser temperature is regulated at 18 K, while 1076 the liquid in the cell cools to about 20.1 K. The latter temperature is 1 K 1077 below the saturation temperature of H<sub>2</sub>, which eliminates boiling within the 1078 cell and permits a more accurate determination of the fluid density,  $71.2 \pm$ 1079  $0.3 \text{ mg/cm}^3$ . The system can be cooled from room temperature and filled with 1080 liquid hydrogen in approximately six hours. Prior to measurements using an 1081 empty target cell, the liquid hydrogen is boiled back into the storage tanks in 1082 about five minutes.  $H_2$  gas continues to condense and drain towards the target 1083 cell, but the condensed hydrogen is immediately evaporated by the cell heater. 1084 In this way, the cell does not warm above 40 K and can be re-filled with liquid 1085 hydrogen in about twenty minutes. 1086

Operation of the cryotarget is highly automated, requires minimal user inter-1087 vention, and has operated in a very reliable and predictable manner throughout 1088 the experiment. The target controls<sup>39</sup> are handled by a LabVIEW program, 1089 while a standard EPICS softIOC running in Linux provides a bridge between 1090 the controller and JLab's EPICS environment (see Section 11). Temperature 1091 readback and control of the condenser and target cell thermometers are man-1092 aged by a four-input temperature controller<sup>40</sup> with PID control loops of 50 and 1093 100 W. Strain gauge pressure sensors measure the fill and return pressures with 1094 0.25% accuracy. When filled with subcooled liquid, the long-term tempera-1095 ture  $(\pm 0.2 \text{ K})$  and pressure  $(\pm 0.1 \text{ psi})$  stability of the liquid hydrogen enable a 1096 determination of the density to better than 0.5%. 1097

<sup>&</sup>lt;sup>39</sup>The control logic uses National Instruments CompactRIO 9030.

 $<sup>^{40}\</sup>mathrm{Lake}$  Shore Model 336.



Figure 15: Cross-section through the cylindrically symmetric Central Drift Chamber, along the beamline.

## <sup>1098</sup> 5. Tracking detectors

## 1099 5.1. Central drift chamber

The Central Drift Chamber (CDC) is a cylindrical straw-tube drift chamber 1100 which is used to track charged particles by providing position, timing and energy 1101 loss measurements [39, 40]. The CDC is situated inside the Barrel Calorimeter, 1102 surrounding the target and Start Counter. The active volume of the CDC 1103 is traversed by particles coming from the hydrogen target with polar angles 1104 between  $6^{\circ}$  and  $168^{\circ}$ , with optimum coverage for polar angles between  $29^{\circ}$ 1105 and 132°. The CDC contains 3522 anode wires of 20  $\mu$ m diameter gold-plated 1106 tungsten inside Mylar<sup>41</sup> straw tubes of diameter 1.6 cm in 28 layers, located in 1107 a cylindrical volume which is 1.5 m long, with an inner radius of 10 cm and 1108 outer radius of 56 cm, as measured from the beamline. Readout is from the 1109 upstream end. Fig. 15 shows a schematic diagram of the detector. 1110

The straw tubes are arranged in 28 layers; 12 layers are axial, and 16 layers are at stereo angles of  $\pm 6^{\circ}$  to provide position information along the beam direction. The stereo angle was chosen to balance the extra tracking information provided by the unique combination of stereo and axial straws along a trajectory against the size of the unused volume inside the chamber at each transition between stereo and axial layers. Fig. 16 shows the CDC during construction.

The volume surrounding the straws is enclosed by an inner cylindrical wall of 0.5 mm G10 fiberglass, an outer cylindrical wall of 1.6 mm aluminum, and two circular endplates. The upstream endplate is made of aluminum, while the downstream endplate is made of carbon fiber. The endplates are connected by 12

<sup>&</sup>lt;sup>41</sup>www.mylar.com


Figure 16: The Central Drift Chamber during construction. A partially completed layer of stereo straw tubes is shown, surrounding a layer of straw tubes at the opposite stereo angle. Part of the carbon fiber endplate, two temporary tension rods and some of the 12 permanent support rods linking the two endplates can also be seen.

aluminum support rods. Holes milled through the endplates support the ends of 1121 the straw tubes, which were glued into place using several small components per 1122 tube, described more fully in [40]. These components also support the anode 1123 wires, which were installed with 30 g tension. At the upstream end, these 1124 components are made of aluminum and were glued in place using conductive 1125  $epoxy^{42}$ . This attachment method provides a good electrical connection to the 1126 inside walls of the straw tubes, which are coated in aluminum. The components 1127 at the downstream end are made of Noryl plastic<sup>43</sup> and were glued in place using 1128 conventional non-conductive epoxy<sup>44</sup>. The materials used for the downstream 1129 end were chosen to be as lightweight as feasible so as to minimize the energy 1130 loss of charged particles passing through them. 1131

At each end of the chamber, a cylindrical gas plenum is located outside the 1132 endplate. The gas supply runs in 12 tubes through the volume surrounding the 1133 straws into the downstream plenum. There the gas enters the straws and flows 1134 through them into the upstream plenum. From the upstream plenum the gas 1135 flows into the volume surrounding the straws, and from there the gas exhausts 1136 to the outside, bubbling through small jars of mineral oil. The gas mixture 1137 used is 50% argon and 50% carbon dioxide at atmospheric pressure. This gas 1138 mixture was chosen since its drift time characteristics provide good position 1139

<sup>&</sup>lt;sup>42</sup>TIGA 920-H, www.loctite.com

 $<sup>^{43}</sup>$ www.sabic.com

<sup>&</sup>lt;sup>44</sup>3M Scotch-Weld DP460NS, www.3m.com

resolution [39]. A small admixture (approximately 1%) of isopropanol is used to prevent loss of performance due to aging[41, 42]. Five thermocouples are located in each plenum and used to monitor the temperature of the gas. The downstream plenum is 2.54 cm deep, with a sidewall of ROHACELL<sup>45</sup> and a final outer wall of aluminized Mylar film, and the upstream plenum is 3.18 cm deep, with a polycarbonate sidewall and a polycarbonate disc outer wall.

The readout cables pass through the polycarbonate disc and the upstream 1146 plenum to reach the anode wires. The cables are connected in groups of 20 to 24 1147 to transition boards mounted onto the polycarbonate disc; the disc also supports 1148 the connectors for the high-voltage boards. Preamplifiers [43] are mounted 1149 on the high-voltage boards. The aluminum endplate, outer cylindrical wall of 1150 the chamber, aluminum components connecting the straws to the aluminum 1151 endplate and the inside walls of the straws are all connected to a common 1152 electrical ground. The anode wires are held at +2.1 kV during normal operation. 1153

# 1154 5.2. Forward Drift Chamber

The Forward Drift Chamber (FDC) consists of 24 disc-shaped planar drift 1155 chambers of 1 m diameter [44]. They are grouped into four packages inside 1156 the bore of the spectrometer magnet. Forward tracking requires good multi-1157 track separation due to the high particle density in the forward region. This is 1158 achieved via additional cathode strips on both sides of the wire plane allowing 1159 for a reconstruction of a space point on the track from each chamber. The FDC 1160 registers particles emitted into polar angles as low as  $1^{\circ}$  and up to  $10^{\circ}$  with all 1161 the chambers, while having partial coverage up to  $20^{\circ}$ . 1162

One FDC chamber consists of a wire plane with cathode planes on either sides at a distance of 5 mm from the wires (Fig. 17). The frame that holds the wires is made out of ROHACELL with a thin G10 fiberglass skin in order to minimize the material and allow low energy photons to be detected in the outer electromagnetic calorimeters.

The wire plane has sense (20  $\mu$ m diameter) and field (80  $\mu$ m) wires 5 mm 1168 apart, forming a field cell of  $10 \times 10$  mm<sup>2</sup>. To reduce the effects of the magnetic 1169 field, a "slow" gas mixture of 40% Ar and 60% CO<sub>2</sub> is used. A positive high 1170 voltage of about 2.2 kV is applied to the sense wires and a negative high voltage 1171 of 0.5 kV to the field wires. The cathodes are made out of  $2-\mu$ m-thin copper 1172 strips on Kapton foil with a pitch of 5 mm, and are held at ground potential. 1173 The strips on the two cathodes are arranged at  $30^{\circ}$  relative to each other and 1174 at angles of  $75^{\circ}$  and  $105^{\circ}$  angle with respect to the wires. 1175

<sup>1176</sup> The six chambers of a package are separated by thin aluminized Mylar. Each <sup>1177</sup> chamber is rotated relative to the previous one by 60°. The total material of a <sup>1178</sup> package in the sensitive area corresponds to 0.43% radiation lengths, with about <sup>1179</sup> half of that in the area along the beam line that has no copper on the cathodes. <sup>1180</sup> The sense wires in the inner area of 6 - 7.8 cm diameter (depending on the <sup>1181</sup> distance of the package to the target) are increased in thickness from 20  $\mu$ m

<sup>&</sup>lt;sup>45</sup>www.rohacell.com



Figure 17: Artist rendering of one FDC chamber showing components. From top to bottom: upstream cathode, wire frame, downstream cathode, ground plane that separates the chambers. The diameter of the active area is 1 m.

to  $\sim 80 \ \mu$ m, which makes them insensitive to the high rates along the beam. The distance between the first and last package is 1.69 m. All chambers are supplied with gas in parallel. In total, 2, 304 wires and 10, 368 strips are read using charge preamplifiers with 10 ns peaking time, with a gain of 0.77 mV/fC for the wires and 2.6 mV/fC for the strips.

# 1187 5.3. Electronics

The high voltage (HV) supply units used are CAEN A1550P<sup>46</sup>, with noisereducing filter modules added to each crate chassis. The low voltage (LV) supplies are Wiener MPOD MPV8008<sup>47</sup>. The preamplifiers are a custom JLab design based on an ASIC [43] with 24 channels per board; the preamplifiers are charge-sensitive, capacitively coupled to the wires in the CDC and FDC, and directly coupled to strips in the FDC.

Pulse information from the CDC anode wires and FDC cathode strips are obtained and read out using 72-channel 125 MHz flash ADCs (FADCs) [45, 46]. These use Xilinx<sup>48</sup> Spartan-6 FPGAs (XC6SLX25) for signal digitization and data processing with 12 bit resolution. Each FADC receives signals from three

<sup>&</sup>lt;sup>46</sup>www.caen.it

<sup>&</sup>lt;sup>47</sup>www.wiener-d.com

 $<sup>^{48}</sup>$ www.xilinx.com

preamplifiers. The signal cables from different regions of the drift chambers are distributed between the FADCs in order to share out the processing load as evenly as possible.

The FADC firmware is activated by a signal from the GLUEX trigger. The 1201 firmware then computes the following quantities for pulses observed above a 1202 given threshold within a given time window: pulse number, arrival time, pulse 1203 height, pulse integral, pedestal level preceding the pulse, and a quality factor 1204 indicating the accuracy of the computed arrival time. Signal filtering and inter-1205 polation are used to obtain the arrival time to the nearest 0.8 ns. The firmware 1206 performs these calculations both for the CDC and FDC alike, and uses different 1207 readout modes to provide the data with the precision required by the separate 1208 detectors. For example, the CDC electronics read out only one pulse but require 1209 both pulse height and integral, while the FDC electronics read out up to four 1210 pulses and do not require a pulse integral. 1211

The FDC anode wires are read out using the JLab pipeline F1 TDC[47] with a nominal least count of 120 ps.

### 1214 5.4. Gas system

Both the CDC and FDC operate with the same gases, argon and  $CO_2$ . Since 1215 the relative mixture of the two gases is slightly different for the two tracking 1216 chambers, the gas system has two separate but identical mixing stations. There 1217 is one gas supply of argon and  $CO_2$  for both mixing stations. A limiting opening 1218 in the supply lines provides over-pressure protection to the gas system, and 1219 filters in the gas lines provide protection against potential pollution of the gas 1220 from the supply. Both gases are mixed using mass flow controllers (MFCs) that 1221 can be configured to provide the desired mixing ratio of argon and CO<sub>2</sub>. MFCs 1222 and control electronics from BROOKS Instruments<sup>49</sup> are used throughout. 1223

The mixed gas is filled into storage tanks, with one tank for the CDC and 1224 another for the FDC. The pressures are regulated by controlling the operation of 1225 the MFCs with a logic circuit based on an Allen-Bradley ControlLogix system<sup>50</sup> 1226 that keeps the pressure in the tank between 10 and 12 psi. The tank serves both 1227 as a reservoir and a buffer. A safety relief valve on each tank provides additional 1228 protection against over-pressure. While the input pressure to the MFC is at 1229 40 psi, the pressure after the MFC is designed to always be less than 14 psi 1230 above atmospheric pressure. After the mixing tank, a provision is built into the 1231 system to allow the gas to pass through an alcohol bath to add a small amount 1232 of alcohol gas to the gas mixture. This small admixture of alcohol protects the 1233 wire chambers from aging effects caused by radiation exposure from the beam. 1234 This part of the gas system is located above ground in a separate gas shed, 1235 before the gas mixture is transported to the experimental hall via polyethylene 1236 pipes. 1237

 $<sup>^{49}\</sup>mathrm{BROOKS}$  Instruments, https://www.brooksinstrument.com/en/products/mass-flow-controllers.

<sup>&</sup>lt;sup>50</sup>Allen-Bradley, https://ab.rockwellautomation.com/

Additional MFCs in the hall allow the exact amount of gas provided to the 1238 chambers to be specified: one MFC for the CDC and another four MFCs for the 1239 individual FDC packages. The CDC is operated with a flow of 1.0 l/m, while 1240 each FDC package is operated with a flow of 0.1 l/m. To protect the chambers 1241 from over-pressure, there is a bypass line at the input to the detectors that is 1242 open to the atmosphere following a bubbler containing mineral oil. The height 1243 of the oil level determines the maximum possible gas pressure at the input to the 1244 chambers. There is a second bubbler at the output to protect against possible 1245 air back-flow into the chamber. The height of the oil above the exhaust line 1246 determines the operating pressure inside the chambers. 1247

Valves are mounted at many locations in the gas system to monitor various pressures with a single pressure sensor. The pressures of all six FDC chambers are monitored, as well as the CDC gas at the input, downstream gas plenum and the exhaust. A valve in the exhaust line can be used to divert some gas from the chamber to an oxygen sensor. Trace quantities of oxygen will reduce the gas gain and reduce tracking efficiency. The oxygen levels in the chamber are below 100 ppm.

#### <sup>1255</sup> 5.5. Calibration, performance and monitoring

Time calibrations for the drift chambers are used to remove the time offset due to the electronics, so that after calibration the earliest possible arrival time of the pulse signals is at 0 ns. These offsets and the function parameters used to describe the relationship between the pulse arrival time and the closest distance between the track and the anode wire are obtained for each session of data taking.

The CDC measures the energy loss, dE/dx, of tracks over a wide range of 1262 polar angles, including recoiling target protons as well as more forward-going 1263 tracks. Gain calibrations are made to ensure that dE/dx is consistent between 1264 tracking paths through different straws and stable over time. The procedure 1265 entails matching the position of the minimum ionizing peak for each of the 3522 1266 straws, and then matching the dE/dx at 1.5 GeV/c to the calculated value of 1267 2.0 keV/cm. This takes place during the early stages of data analysis. Gain 1268 calibration for the individual wires is performed each time the HV is switched 1269 on and whenever any electronics modules are replaced. Gain calibration for the 1270 chamber as a whole is performed for each session of data taking; these sessions 1271 are limited to two hours as the gain is very sensitive to the atmospheric pressure. 1272 Position calibrations were necessary to describe the small deflection of the straw 1273 tubes midway along their length; these were performed in 2016 and repeated 1274 in 2017, with no significant difference found between the two sets of results. 1275 Position resolution from the CDC is of the order of 130  $\mu$ m and its detection 1276 efficiency per straw is over 98% for tracks up to 4 mm from the CDC wire. The 1277 efficiency decreases as the distance between the track and the wire increases, 1278 but the close-packing arrangement of the straw tubes and the large number of 1279 straws traversed by each track compensate for this. 1280

For the FDC system, an internal per-chamber calibration process is first performed to optimize the track position accuracy. In the FDC the avalanche



Figure 18: Wire (avalanche) positions reconstructed from the strip information on the two cathodes in one FDC chamber. Only one quarter of the chamber is shown in this figure.

created around the wire is seen in three projections: on the two cathodes and on 1283 the wires. The drift time information from the wires is used to reconstruct the 1284 hit position perpendicular to the wire. The strip charges from the two cathodes 1285 are used to reconstruct the avalanche position along the wire. The same strip 1286 information can be used to reconstruct the avalanche position perpendicular to 1287 the wire, which, due to the proximity of the avalanche to the wire, is practically 1288 the wire position, as illustrated in Fig 18. This strip information is used to 1289 align the strips on the two cathodes with respect to the wires. At the same 1290 time, the residuals of the reconstructed wire positions are an estimate of the 1291 strip resolution. The resolutions of the detector were reported earlier [44]. The 1292 strip resolution along the wires, estimated from the wire position reconstruction, 1293 varies between 180 and 80  $\mu$ m, depending on the total charge induced on the 1294 strips. The drift distance is reconstructed from the drift time with a resolution 1295 between 240 and 140  $\mu$ m depending on the distance of the hit to the wire in the 1296 0.5 - 4.5 mm range. 1297

Position offsets and package rotations were determined for both drift chamber systems, first independently, and then together, using the alignment software

#### <sup>1300</sup> MILLEPEDE[48] in a process described in [40] and in [49].

<sup>1301</sup> Online monitoring software enables shift-takers to check that the number of <sup>1302</sup> channels recording data, the distribution of signal arrival times, and the dE/dx<sup>1303</sup> distribution are as expected.

#### <sup>1304</sup> 6. Performance of the charged-particle-tracking system

### 1305 6.1. Track reconstruction

The first stage in track reconstruction is pattern recognition. Hits in adjacent 1306 layers in the FDC in each package are formed into track segments that are linked 1307 together with other segments in other packages to form FDC track candidates 1308 using a helical model for the track parameters. Hits in adjacent rings in the axial 1309 layers of the CDC are also associated into segments that are linked together with 1310 other segments in other axial layers and fitted with circles in the projection 1311 perpendicular to the beam line. Intersections between these circles and the 1312 stereo wires are found and a linear fit is performed to find a z-position near the 1313 beamline and the tangent to the dip angle  $\lambda = \pi/2 - \theta$ . These parameters, in 1314 addition to the circle fit parameters, form a CDC track candidate for each set 1315 of linked axial and stereo layers. Candidates that emerge from the target, and 1316 pass through both FDC and CDC in the  $5^{\circ} - 20^{\circ}$  range, are linked together. 1317

The second stage uses a Kalman filter [50, 51] to find the fitted track param-1318 eters  $\{z, D, \phi, \tan \lambda, q/p_T\}$  at the position of closest approach of the track to the 1319 beam line. The track candidate parameters are used as an initial guess, where 1320 D is the signed distance of closest approach to the beam line. The Kalman filter 1321 proceeds in steps from the hits farthest from the beam line toward the beam 1322 line. Energy loss and multiple scattering are taken into account at each step 1323 along the way, according to a map of the magnetic field within the bore of the 1324 solenoid magnet. For the initial pass of the filter, the drift time information 1325 from the wires is not used. Each particle is assumed to be a pion, except for low 1326 momentum track candidates (p < 0.8 GeV/c), for which the fits are performed 1327 with a proton hypothesis. 1328

The third stage matches each fitted track from the second stage to either the Start Counter, the Time-of-Flight scintillators, the Barrel Calorimeter, or the Forward Calorimeter to determine a start time t0 so that the drift time to each wire associated with the track could be used in the fit. Each track is refitted with the drift information, separately for each value of mass for particles in the set  $\{e^{\pm}, \pi^{\pm}, K^{\pm}, p^{\pm}\}$ .

### 1335 6.2. Momentum and vertex resolution

The momentum resolution as a function of angle and magnitude for pions and protons is shown in Fig. 19. The angular resolution is shown in Fig. 20.

The thin windows of the cryogenic target and the exit window of the target vacuum chamber provide a means to estimate the vertex resolution of the tracking system. Pairs of tracks from empty target measurements are used to



Figure 19: (Left) Momentum resolution for  $\pi^-$  tracks. (Right) Momentum resolution for proton tracks.



Figure 20: (Left) Polar angle resolution for  $\pi^-$  tracks. (Right) Azimuthal angle resolution for  $\pi^-$  tracks. The resolutions are plotted as a function of the polar angle,  $\theta$ .



Figure 21: Reconstructed vertex positions within 1 cm radial distance with respect to the beam line for an empty target measurement. The curve shows the result of a fit to the vertex distribution used to determine the vertex resolution.

reconstruct these windows as illustrated in Fig. 21. The distance of closest approach between two tracks, d, was required to be less than 1 cm. The vertex position is at the mid-point of the line segment (of length d) defined by the points of closest approach for each track. The estimated z-position resolution is 3 mm.

# 1346 7. Electromagnetic calorimeters

#### <sup>1347</sup> 7.1. Barrel Calorimeter

The Barrel Calorimeter (BCAL) is an electromagnetic sampling calorime-1348 ter in the shape of an open cylinder. Photon showers with energies between 1349 0.05 GeV and several GeV,  $11^{\circ}-126^{\circ}$  in polar angle, and  $0^{\circ}-360^{\circ}$  in azimuthal 1350 angle are detected. The geometry is fairly unique with the production target 1351 located in the backward part of the cylinder, as shown in Fig. 1. The contain-1352 ment of showers depends on the angle of photon incidence, with a thickness of 1353 15.3 radiation lengths for particles entering normal to the calorimeter face and 1354 reaching up to 67 radiation lengths at 14°. Details of the design, construction 1355 and performance of the BCAL can be found in Ref. [52]. 1356

The BCAL is constructed as a lead and scintillating-fiber matrix, consisting 1357 of 0.5 mm-thick corrugated lead sheets and 1.0 mm-diameter Kuraray SCSF-1358 78MJ multi-clad scintillating fibers. The fibers run parallel to the cylindrical 1359 axis of the detector. Each module has approximately 185 layers and 15,000 1360 fibers. The BCAL consists of 48 optically isolated modules, each with a trape-1361 zoidal cross section, forming a 3.9-m-long cylindrical shell having inner and 1362 outer radii of 65 cm and 90 cm, respectively. The light generated in the fibers 1363 is collected via small light guides at each end of the module, which transport 1364



Figure 22: Three-dimensional rendition of the light guides mounted at the end of the BCAL, as well as the readout assemblies mounted over them. The readout assemblies contain the SiPMs and their electronics. (Color online)

the light to silicon photomultipliers (SiPMs), which were chosen due to their insensitivity to magnetic fields. The end of the calorimeter with light guides, light sensors and electronics is shown in Fig. 22.

The SiPM light sensors are Hamamatsu S12045(X) Multi-Pixel-Photon Counter 1368 (MPPC) arrays <sup>51</sup>, which are  $4 \times 4$  arrays of  $3 \times 3$  mm<sup>2</sup> tiles [53]. The SiPMs 1369 were accepted following extensive testing [54, 55, 56, 57, 58, 59]. Four thousand 1370 units were purchased and 3840 are installed in the detector. The gain of the 1371 SiPM depends on the voltage above the breakdown voltage, about 70 V. These 1372 are operated at 1.4 V over the breakdown voltage, selected to reduce the effect 1373 of readout thresholds. Even at this relatively high over-bias, the noise level is 1374 dominated by fluctuations in the electronics baseline and not by single-pixel 1375 noise. In order to keep a constant gain, the temperature is maintained within 1376 practical limits  $(\pm 2^{\circ}C)$  using a chilled-water system. The gain is stabilized 1377 using a custom circuit that adjusts the bias voltage based on the measured tem-1378 perature. Two stages of preamplifiers and summing electronics are attached to 1379 the sensors. In order to reduce the number of signals that are digitized, circuits 1380

<sup>&</sup>lt;sup>51</sup>Hamamatsu Corporation, Bridgewater, NJ 08807, USA (http://sales.hamamatsu.com/en/home.php).



Figure 23: Expanded view of a single FCAL module.

<sup>1381</sup> sum the outputs of the preamplifiers in groups of radial columns, with coarser <sup>1382</sup> granularity away from the target. The layer closest to the target employs a <sup>1383</sup> single SiPM, and the next three layers have two, three, and four SiPMs, respec-<sup>1384</sup> tively. On the end of each module, forty SiPMs generate sixteen signals that are <sup>1385</sup> delivered to FADCs and twelve signals that are discriminated and then recorded <sup>1386</sup> with pipeline TDCs. The FADCs and TDCs are housed in VXS crates located <sup>1387</sup> on the floor close to the detector (see Section 9).

# 1388 7.2. Forward Calorimeter

The Forward Calorimeter (FCAL) detects photon showers with energies 1389 ranging from 0.1 GeV to several GeV, and between 1°-11° in polar angle. The 1390 front face of the FCAL is located 5.6 m downstream from the center of the 1391 GlueX target and consists of 2800 lead glass blocks stacked in a circular array 1392 that has a diameter of 2.4 m. Each lead glass block has transverse dimensions 1393 of  $4 \times 4$  cm<sup>2</sup> and length of 45 cm. The material of the lead-glass blocks is equiv-1394 alent to type F8 manufactured by the Lytkarino Optical Glass Factory.<sup>52</sup> The 1395 blocks and most of the PMTs were taken from the decommissioned experiments 1396 E852 at Brookhaven National Laboratory [60] and the RadPhi Experiment at 1397 JLab [61]. To remove accumulated radiation damage, the glass was annealed 1398 by heat treatment prior to installation in GLUEX. The detector is enclosed in a 1399 dark room. 1400

The light collection is accomplished via an Eljen EJ-560 optical interface "cookie" and a UVT acrylic cylindrical light guide glued to the PMT. The light guide recesses the magnetically sensitive photocathode of the PMT inside a dual layer of soft iron and mu-metal that attenuates the stray field of the GLUEX solenoid ( $\leq 200$  G). The sensors are FEU 84-3 PMTs with Cockcroft-Walton bases, each consuming 0.2 W. The design of the PMT base is similar to that

 $<sup>^{52}\</sup>mathrm{http://lzos.ru}$  .

noted in Ref. [62], and eliminates the need for a 2800-channel high-voltage power
system. The bases communicate with a controller using the CAN protocol [63],
with 100 bases on each of 28 CAN buses. The communication allows continuous
monitoring of the PMT voltages, temperatures, and current draw. A schematic
of a single FCAL module is shown in Fig. 23 and more details may be found in
Ref. [64]. FCAL signals are routed to FADC electronics, situated on a platform,
directly behind the FCAL dark room.

## 1414 7.3. Electronics

Custom readout electronics for the two calorimeters are mounted in standard 1415 VXS crates and include JLab 12-bit 250 MHz FADCs [65], discriminators [66] 1416 and F1 TDCs [47]. The maximum input scale of the FADCs (4095 counts) is set 1417 to 2 V. The FADCs sample each calorimeter channel every 4 ns and generate 1418 raw waveforms consisting of 100 samples (400 ns). The samples are available 1419 for further processing by the firmware upon a trigger signal, if the waveform 1420 exceeds a threshold voltage. The firmware computes several derived quantities 1421 of the pulse: pedestal, peak value, integral over a selected window, and time 1422 of the halfway point on the leading edge. At most one pulse is extracted from 1423 each readout window. These pulse features constitute the raw data that is 1424 nominally read out from the FADC. Optionally, the full waveforms can be read 1425 out for diagnostic purposes and to check the firmware output against the offline 1426 emulation of the parameter extraction; this is done for less than about 1% of 1427 the production runs. 1428

Pulses are identified by the first sample that exceeds a threshold, currently 1429 set to 5 (8) counts above the average pedestal for the BCAL (FCAL). These 1430 thresholds correspond to approximately 2.5 (12) MeV. The integral is deter-1431 mined using a fixed number of samples relative to the threshold crossing, which 1432 was determined by maximizing the ratio of signal to pedestal noise. The inte-1433 gration window begins one sample before the threshold time and extends to 26 1434 (15) samples after the threshold time for the BCAL (FCAL). Typical pedestal 1435 widths are  $\sigma \sim 1.2$ -1.3 (0.8) counts. For the BCAL, the pedestals are determined 1436 for each channel event-by-event, appropriately scaled, and then subtracted from 1437 the peak and integral to obtain signals proportional to the energy deposited in 1438 the calorimeter. For the FCAL, the average pedestal over a run period is deter-1439 mined offline for each channel and the pedestal contribution to the pulse integral 1440 is subtracted when the data are reconstructed. The algorithm that determines 1441 the time of the pulse is pulse-height independent and, therefore, time-walk cor-1442 rection is not required for the FADC times [67]. 1443

The outputs of the three inner layers of the BCAL are also fanned out to leading-edge discriminators, which feed the JLab F1 TDCs. The discriminator thresholds are initially set to 35 mV and then adjusted channel by channel. The pulse times are recorded relative to the trigger in a 12-bit word. Multiple hits may be recorded per channel per event (up to eight), but are culled at a later time by comparison to FADC times. The nominal least count is configured to be 58 ps.

### 1451 7.4. Calibration and monitoring

The relative gains of the calorimeters are monitored using a modular LED-1452 driver system [68]. The control system is the same for both calorimeters, but 1453 the arrangement of LEDs is tailored to the respective detector geometries. In 1454 the BCAL, one LED is inserted into each light guide to monitor each individual 1455 SiPM and its partner at the far end of the module. Due to geometry, the 1456 illumination varies considerably from channel to channel. The average gain 1457 stability of the detector over a period of ten days is better than 1% and the 1458 fractional root-mean-square deviation of the mean for each SiPM during a single 1459 day from the average over the run period is typically less than 2%. 1460

For the FCAL, four acrylic panes were installed, each covering the upstream 1461 end of one quadrant of the FCAL. Each pane is illuminated by forty LEDs, ten 1462 violet, ten blue, and twenty green. In addition to monitoring the stability of 1463 the readout, the different colors are used to study the wavelength dependence of 1464 the transmission of light though the lead glass blocks. In particular, radiation 1465 damage to lead glass inhibits transmission at the blue end of the spectrum 1466 and tends to turn glass a brownish color [69]. Throughout a several-month 1467 experiment, the response to the green LEDs was unchanged. However, the PMT 1468 response to violet LEDs degraded by about 10% in the blocks closest to the beam 1469 line, characteristic of radiation damage. Such damage is only evident in the first 1470 two layers of blocks surrounding the 12 cm  $\times$  12 cm beam hole. This damage is 1471 likely confined to the upstream end of the block and does not significantly affect 1472 the response to particle showers in the body of the glass. 1473

The energy of a photon or lepton is obtained from the reconstructed electro-1474 magnetic shower. Here, a shower is reconstructed using an algorithm that finds 1475 a cluster by grouping signals close in time and space, called hits, that have been 1476 registered by individual detector elements. Details of the algorithms to obtain 1477 shower energies in the BCAL can be found in Ref. [52] and in Ref. [70] for the 1478 FCAL. The clustering in the FCAL requires that hits register within 15 ns of 1479 the primary hit, where the seed threshold is taken to be 35 MeV. Clusters with a 1480 single hit are discarded. In the event of overlapping showers, the hit energies are 1481 divided among the clusters in proportion to the partition predicted by a typical 1482 shower profile. Both detectors have sources of energy-dependent nonlinearities 1483 and empirical corrections are developed and applied to minimize the measured 1484 energy dependence of the measured  $\pi^0$  mass. 1485

# 1486 7.5. Performance

The performance of the calorimeter is summarized by its ability to measurethe energy, position and timing of electromagnetic showers.

The energy resolution of each calorimeter was extracted from the measured  $\pi^{0}$  and  $\eta$  mass distributions, yielding consistent results. To study the  $\eta$  mass resolution, events were selected using kinematic fits to  $\gamma p \rightarrow p\pi^{+}\pi^{-}\gamma\gamma$ , with  $\eta \rightarrow \gamma\gamma$  and the photons having the same energies within 10%. The proton and pion tracks were used to determine the event vertex, needed to accurately reconstruct the two-photon invariant mass. This reaction provides a fairly clean

sample of  $\eta$ 's with energy-symmetric photons recorded either both in the BCAL 1495 or both in the FCAL. The single-photon energy resolution was determined from 1496 Gaussian fits to the  $\eta$  invariant mass width, neglecting contributions from uncer-1497 tainty in the opening angle. Monte Carlo simulation of  $\gamma p \to p \pi^+ \pi^- \eta$  events, 1498 with kinematics chosen to approximate the experimental distributions, were 1499 used to tune the MC resolution to match the data. The single-photon resolu-1500 tions are shown in Fig. 24(a) for the BCAL and Fig. 24(b) for the FCAL as a 1501 function of the mean photon energy, both for data and simulation. A fit has 1502 been performed to the data for each calorimeter to estimate contributions to 1503 the width from stochastic and constant processes. The parameters in the fit are 1504 strongly correlated due to the limited range of energy available.<sup>53</sup> 1505

The resolution of the position (Z) along the length of the BCAL (~2.5 cm) is computed from the timing resolution of the system, which was measured to be  $\sigma = 150 \text{ ps}$  at 1 GeV. The transverse position resolution ( $\sigma$ ) obtained from simulation for 1 GeV showers in the FCAL is less than 1.1 cm.

The performance of the calorimeters has been demonstrated in the reconstruction of neutral states including  $\pi^0$ ,  $\eta$  and  $\eta'$  mesons for the first GLUEX physics publications [71, 72]. In addition, although the response of the calorimeters at high energy is still under evaluation, it has provided important electronpion separation to identify the decays of  $J/\psi \rightarrow e^+e^-$  [73] where electrons were recorded up to 8 GeV.



Figure 24: The energy resolution,  $\sigma_{\gamma}/E_{\gamma}$ , for single photons in the a) BCAL and b) FCAL calculated from the  $\eta$  mass distribution under the assumption that only the energy resolution contributes to its width. Solid black circles are data and open red squares are simulation. Fitted curves including the stochastic and constant terms are indicated. (Color online)

### <sup>1516</sup> 8. Scintillation detectors

<sup>1517</sup> There are two scintillator-based detectors deployed in the GLUEX spectrom-<sup>1518</sup> eter: a small barrel-shaped detector surrounding the target, referred to as the

 $<sup>^{53}</sup>$ For the BCAL these data constitute an average over many angles, resulting in a relatively large effective constant term that cannot be extrapolated to higher energy. See Ref. [52] Section 11 for details.

Start Counter (ST), and a two-plane hodoscope detector system in the forward direction, referred to as the Time-of-Flight (TOF) detector. Both detectors provide timing information. Charged-particle identification is derived from energy loss (dE/dx) in the ST and flight time from the TOF.

# 1523 8.1. Start Counter

The ST, shown in Fig. 25, surrounds the target region and covers about 90%1524 of the solid angle for particles originating from the center of the target. The ST 1525 is designed to operate at tagged photon beam intensities of up to  $10^8$  photons per 1526 second in the coherent peak, and has a high degree of segmentation to limit the 1527 per-paddle rates. The time resolution must be sufficient to resolve the RF beam 1528 structure and identify the electron beam bunch from which the event originated 1529 (see Section 2.1). The ST provides a timing signal that is relatively independent 1530 of particle type and trajectory (because of its proximity to the target) and can 1531 be used in the Level 1 trigger if necessary. The specific energy deposits dE/dx1532 in ST are used for charged-particle identification in combination with the flight-1533 time from the TOF. Details of the design, construction and performance of the 1534 ST system can be found in Ref. [74]. 1535



Figure 25: The GLUEX Start Counter surrounding the liquid-hydrogen target assembly. The incident beam travels from left to right down the central axis.

The ST consists of 30 scintillator paddles arranged in a cylinder of radius 78 mm with a "nose" section that bends towards the beam line to a radius of

20 mm at the downstream end. EJ-200 scintillator from Eljen Technology<sup>54</sup> 1538 was selected for the ST paddles. EJ-200 has a decay time of 2.1 ns with a bulk 1539 attenuation length of 380 cm. Each scintillator paddle originated from stock 1540 3 mm thick and 600 mm in length. The paddles were bent at Eljen to create 1541 the nose section, and then machined at McNeal Enterprises Inc.<sup>55</sup> to their 1542 final shape, including edges beveled at  $6^{\circ}$  to minimize loss of acceptance. The 1543 scintillator paddles are supported by a Rohacell closed-cell foam structure. The 1544 Rohacell is 11 mm thick and is rigidly attached to an aluminum support hub 1545 at the upstream end. The downstream support extends partially into the nose 1546 section. The cylindrical length of the Rohacell is further reinforced with three 1547 layers of carbon fiber, each layer being 650  $\mu$ m thick. The assembly is made 1548 light-tight with a Tedlar wrapping, attached to a plastic collar at the upstream 1549 end. 1550

Silicon photomultiplier detectors are used as light sensors, as these are not affected by the magnetic field produced by the solenoid. The SiPMs were placed at the upstream end of each scintillator element with a 250  $\mu$ m air gap. Each paddle is read out with an array of four SiPMs (Hamamatsu S109031-050P multi-pixel photon counters) whose signals are summed. The on-board electronics provides two signals per paddle, one delivered to an FADC, and the other to a 5× amplifier that is sent to a discriminator and then to a TDC.

#### 1558 8.2. Time-of-flight counters

The TOF system delivers fast timing signals from charged particles passing 1559 through the detector, thereby providing information for particle identification. 1560 The TOF detector is a wall of scintillators located about 5.5 m downstream from 1561 the target, covering a polar angular region from  $0.6^{\circ}$  to  $13^{\circ}$ . The detector has 1562 two planes of scintillator paddles stacked in the horizontal and vertical direction. 1563 Most paddles are 252 cm long and 2.54 cm thick with a width of 6 cm. The 1564 scintillator material is EJ-200 from Eljen Technology. To allow the photon 1565 beam to pass through the central region, an aperture of  $12 \times 12$  cm<sup>2</sup> is kept free 1566 of any detector material by using four shorter, single-PMT paddle detectors 1567 with a length of 120 cm around the beam hole in each detector plane. These 1568 paddles also have a width of 6 cm and a thickness of 2.54 cm. In order to keep 1569 the count rate of the paddles well below 2 MHz the two innermost full-length 1570 paddles closest to the beam hole on either side have a reduced width of 3 cm. 1571 Light guides built out of UV transmitting plastic provide the coupling between 1572 the scintillator and the PMT and allow the magnetic shielding to protect the 1573 photocathode by extending about 5 cm past the PMT entrance window. All 1574 paddles are wrapped with a layer of a highly reflective material (DF2000MA 1575 from 3M) followed by a layer of strong black Tedlar film for light tightness. 1576

1577

The scintillator paddles are read out using PMTs from Hamamatsu. $^{56}$  Full-

<sup>&</sup>lt;sup>54</sup>Eljen Technology, https://eljentechnology.com/products/plastic-scintillators.

<sup>&</sup>lt;sup>55</sup>McNeal Enterprises Inc., http://www.mcnealplasticmachining.com

<sup>&</sup>lt;sup>56</sup>Hamamatsu Photonics, https://www.hamamatsu.com/us/en/index.html.

<sup>1578</sup> length paddles have a PMT at both ends, while the short paddles have a single <sup>1579</sup> PMT at the outer end of the detector. These type H10534 tubes have ten stages <sup>1580</sup> and are complete assemblies with high voltage base, casing and  $\mu$ -metal shield-<sup>1581</sup> ing. Additional soft-iron external shielding protects each PMT from significant <sup>1582</sup> stray fields from the solenoid magnet.

#### 1583 8.3. Electronics

High voltage for the TOF PMTs is provided by CAEN HV modules of type 1584 A1535SN, initially controlled by a CAEN SY1527 main frame and later up-1585 graded to a SY4527. The PMT outputs are connected to a passive splitter by 1586 a 55'-long RG-58 coaxial cables. The signal is split into two equal-amplitude 1587 signals. One signal is directly connected to a FADC [75], while the second signal 1588 passes first through a leading-edge discriminator and is then used as an input 1589 to a high resolution TDC. The digitizing modules are mounted in VXS crates 1590 as described in Section 9. The threshold of the leading-edge discriminator is 1591 controlled separately for each channel and has an intrinsic deadtime of about 1592 25 ns.1593

The sparsification threshold for the FADC is set to 120 (160) counts for the ST (TOF), with the nominal pedestal set at 100 counts. The high voltage of each TOF PMT is adjusted to generate a signal amplitude of at least 400 ADC counts above baseline from a minimum-ionizing particle. The data from the FADC are provided by the FPGA algorithm and consist of two words per channel with information about pedestal, signal amplitude, signal integral, and timing.

The timing signals from the ST system are registered using the JLab F1 TDCs, which have a nominal least count of 58 ps. In order to take advantage of the higher intrinsic resolution of the TOF counters, this system uses the VX1290A TDCs from CAEN<sup>57</sup>, which are multi-hit high-resolution TDCs with a buffer of up to 8 words per channel and a nominal least count of 25 ps. Since these TDCs provide the best time measurements in the GLUEX detector, the timing of the accelerator RF signal is also digitized using these TDCs.

# 1608 8.4. Calibration and monitoring

The combined ST and TOF systems are used to determine the flight times 1609 of particles, the ST providing a precise start time in combination with the 1610 accelerator RF, and the TOF providing the stop time. Both systems may also 1611 be used to provide information on particle energy loss. Therefore, the signals 1612 in ST and TOF must be calibrated to determine corrections for the effects of 1613 time-walk, light propagation time offsets, and light attenuation. The procedures 1614 are slightly different for the two detectors because of the different geometries, 1615 intrinsic resolutions, and the advantages of the TOF system having two adjacent 1616 perpendicular planes. 1617

<sup>&</sup>lt;sup>57</sup>CAEN, https://www.caen.it/

For the time-walk correction for each paddle of the ST, the detector signal is 1618 sent to both an FADC and a TDC. The time from the FADC, being independent 1619 of pulse amplitude, is the reference. The amplitude dependence of the difference 1620 between TDC and FDC times is used to measure the time walk; the resulting 1621 curve is fit to an empirical function for use in the correction. The propagation 1622 time is measured as a function of the hit position in a paddle as determined 1623 by well-reconstructed charged particle tracks. The propagation velocity is mea-1624 sured in three regions of the counter ("straight," "bend," and "nose") and is not 1625 assumed to be a single value for all hits. The light attenuation is also measured 1626 at several positions along the counter using charged particle tracks. The energy-1627 per-unit pathlength in the paddle as a function of distance from the SiPM is 1628 fit to a modified exponential, with different parameters allowed for the straight 1629 section and the nose section, with continuity enforced at the section boundary. 1630

The calibration procedures for the TOF system take advantage of the two 1631 planes of narrow paddles oriented orthogonal to each other, which permits cal-1632 ibration of the full TOF detector independently of any other external detector 1633 information. The overlap region of two full-length paddles from the two planes 1634 defines a  $6 \times 6$  cm<sup>2</sup> area for most paddles, with a few  $3 \times 3$  cm<sup>2</sup> areas close to 1635 the beam hole. The separation between the two detector planes is minimal as 1636 they are mounted adjacent to each other, separated only by wrapping material. 1637 While the time-difference (TD) between the two ends of a paddle is related to 1638 the hit position along the paddle, the mean-time (MT) is related to the flight 1639 time of a particle from the vertex to the paddle. Therefore, the MT for two 1640 overlapping paddles must be the same when hit by the same particle passing 1641 through both paddles, while the hit positions in the horizontal and vertical di-1642 mensions are defined by the TD of the two paddles. This relationship results 1643 in an internally consistent calibration of all paddles with respect to every other 1644 paddle. Prior to finding timing offsets for calibration, all times are corrected 1645 for the amplitude-dependent walk. The relation between time at threshold and 1646 signal amplitude is parameterized and used to correct for time slewing. 1647

After all full-length paddles have been calibrated, they can be used themselves as references to calibrate the remaining eight short paddles that only have single-ended readout. Again we use the fact that any overlap region of two paddles from different planes has the same particle flight time from the vertex. This coincidence produces peaks in the time difference distributions that can be used to determine the timing offsets of these single-ended readout paddles.

To test the calibration, we take tracks that are incident on a paddle in one plane and compute the time difference between the MT of that paddle and the MT of every other full-length paddle in the other plane. The resulting distribution of these differences is shown in Fig. 26. Assuming that all paddles have the same timing resolution, we can compute the average time resolution to be  $\sigma = 105$  ps=  $\frac{148}{\sqrt{2}}$  ps, assuming a Gaussian distribution.

1660 8.5. Performance

The purpose of the ST is to select the electron beam bunch that generated the tagged photon which induced a reaction in the target. The corresponding



Figure 26: Mean time difference between one TOF long paddle of one plane with all other long paddles of the other plane. (Color online)

time derived from a signal from the CEBAF accelerator, which is synchronized with the RF time structure of the machine, is used to determine the event start time. Therefore, the ST resolution does not contribute to the resolution of the flight time as long as the resolution is sufficient to pick out the correct beam bunch with high probability.

The ST timing performance can be determined by comparing the event time at the target measured by the start counter and the accelerator RF time. The start counter time must be corrected for the flight path of the charged particle emerging from the event, and all instrumental corrections mentioned in the previous section must be applied. Fig. 27 shows the distribution of this time difference. The average time resolution is about  $\sigma=234$  ps, where the resolution varies depending on the position of the hit along the counter.

<sup>1675</sup> The ST is also used to identify particles using dE/dx. Fig. 28 shows dE/dx<sup>1676</sup> versus momentum, p, for charged particles tracked to the Start Counter. Protons <sup>1677</sup> can be separated from pions up to p = 0.9 GeV/c.

<sup>1678</sup> The performance of the TOF detector for particle identification (PID) was <sup>1679</sup> investigated by considering the relative number of particle types within the event <sup>1680</sup> sample. Events with at least three fully-reconstructed positively-charged tracks <sup>1681</sup> were selected, with at least one of these tracks intersecting the TOF detector. <sup>1682</sup> More pions are expected than protons, and more protons than kaons. Looking <sup>1683</sup> at the distribution of velocity,  $\beta$ , of these tracks as a function of momentum, <sup>1684</sup> the bands from protons, kaons and pions are identified (see Fig. 29).

<sup>1685</sup> The distributions of  $\beta$  at two specific track momenta, 2 GeV/c and 4 GeV/c <sup>1686</sup> (see Fig. 30), are illustrative of the PID capability of the TOF detector. At <sup>1687</sup> p = 2 GeV/c, the TOF detector provides about a  $4\sigma$  separation between the <sup>1688</sup> pion/positron peak and the kaon peak, sufficient to identify tracks as kaons



Figure 27: Time difference distribution between the vertex time computed from the start counter and the accelerator RF. The time from the RF does not contribute significantly to the width of the distribution. The fit function is a double Gaussian plus a third-degree polynomial.



Figure 28: dE/dx vs. p for the Start Counter. The curved band corresponds to protons while the horizontal band corresponds to electrons, pions, and kaons. Pion/proton separation is achievable for tracks with p < 0.9 GeV/c.

with  $\beta = 0.97$ , or lower, with very high certainty. However, at  $\beta = 0.98$ , the 1689 probability of the track being a kaon is less than 50%, due to the abundance 1690 of pions that is an order of magnitude larger than kaons. The protons, on the 1691 other hand, are very well separated from the other particle types and can be 1692 identified with high confidence over the full range in  $\beta$ . At a track momentum 1693 of 4 GeV/c, PID becomes much more difficult and represents the limit at which 1694 the time-of-flight measurement can identify protons with high confidence. The 1695 separation between the large peak containing pions, kaons and positrons from 1696 the proton peak is about  $4\sigma$ , while the relative abundance in this case is about 1697 a factor of 4. As a consequence, a 4 GeV/c momentum track with  $\beta = 0.975$ 1698 is most likely a proton, with a small probability of being a pion. At  $\beta = 0.98$ , 1699



Figure 29:  $\beta$  of positive tracks versus track momentum, showing bands for  $e^+$ ,  $\pi^+$ ,  $K^+$  and p. The color coding of the third dimension is in logarithmic scale.(Color online)



Figure 30:  $\beta$  of positive tracks with 2 GeV/c momentum (left) and with 4 GeV/c (right).

<sup>1700</sup> such a track has a similar probability for being a proton or a pion.

# 1701 9. Trigger

The goal of the GLUEX trigger is to accept most high-energy hadronic interactions while reducing the background rate induced by electromagnetic and low-energy hadronic interactions to the level acceptable by the data acquisition system (DAQ). The main trigger algorithm is based on measurements of energy depositions in the FCAL and BCAL as described in Ref. [76, 77]. Supplementary triggers can also use hits from scintillator detectors, such as the PS, tagging detectors, ST, TOF, and TAC.

# 1709 9.1. Architecture

The GLUEX trigger system[78] is implemented on dedicated programmable pipelined electronics modules, designed at JLab using Field-Programmable Gate Arrays (FPGAs). The GLUEX trigger and readout electronics are hosted in VXS (ANSI/VITA 41.0) crates. VXS is an extension of the VME/VME64x architecture, which uses high-speed backplane lines to transmit trigger information.

A layout of the trigger system is presented in Fig. 31. Data from the FCAL 1715 and BCAL are sent to FADC modules [75], situated in 12 and 8 VXS crates, 1716 respectively, and are digitized at the sampling rate of 250 MHz. The digitized 1717 amplitudes are used for the trigger and are also stored in the FPGA-based 1718 pipeline for subsequent readout via VME. Digitized amplitudes are summed for 1719 all 16 FADC250 channels in each 4 ns sampling interval and are transmitted to 1720 the crate trigger processor (CTP) module, which sums up amplitudes from all 1721 FADC boards in the crate. The sub-system processor (SSP) modules located 1722 in the global trigger crate receive amplitudes from all crates and compute the 1723 total energy deposited in the FCAL and BCAL. The global trigger processor 1724 (GTP) module collects data from the SSPs and makes a trigger decision based 1725 on the encoded trigger equations. The core of the trigger system is the trigger 1726 supervisor (TS) module, which receives the trigger information from the GTP 1727 and distributes triggers to the electronics modules in all readout crates in order 1728 to initiate the data readout. The GLUEX system has 55 VXS crates in total (26 1729 with FADC250s, 14 with FADC125s, 14 with F1 TDCs, and 1 CAEN TDC). The 1730 TS also provides a synchronization of all crates and provides a 250 MHz clock 1731 signal. The triggers and clock are distributed through the trigger distribution 1732 (TD) module in the trigger distribution crate. The signals are received by 1733 the trigger interface (TI) module and signal distribution (SD) module in each 1734 crate. The GLUEX trigger system provides a fixed latency. The longest trigger 1735 distribution time of about 3.3  $\mu$ s is due to the distance of the tagger hall from 1736 Hall D. The smallest rewritable readout buffer, where hits from the detector are 1737 stored, corresponds to about 3.7  $\mu$ s for the F1 TDC module. The trigger jitter 1738 does not exceed 4 ns. 1739

# 1740 9.2. Trigger types

The GLUEX experiment uses two main trigger types: the pair spectrometer trigger, and the physics trigger based on energy depositions in the BCAL and FCAL. The pair spectrometer trigger is used to measure the flux of beam photons. This trigger requires a time coincidence of hits in the two arms of the PS detector, described in Section 2.10. The physics triggers are generated when the FCAL and BCAL energies satisfy the following conditions:

1747 1. 
$$2 \cdot E_{\text{FCAL}} + E_{\text{BCAL}} > 1 \text{ GeV}, E_{\text{FCAL}} > 0 \text{ GeV}, \text{ and}$$

1748 1749

2. 
$$E_{\rm BCAL} > 1.2 \, {\rm GeV}.$$

The first condition defines the main trigger that uses the fact that most events produce forward-going energy. The second trigger type is used to accept events with large transverse energy released in the BCAL, such as decays of  $J/\psi$ mesons.

<sup>1754</sup> Several other trigger types were implemented for efficiency studies and de-<sup>1755</sup> tector calibration. Efficiency of the main production trigger was studied using <sup>1756</sup> a trigger based on the coincidence of hits from the ST and TAGH, detectors not <sup>1757</sup> used in the main production trigger. A combination of the PS and TAC triggers <sup>1758</sup> was used for the acceptance calibration of the PS, described in Section 2.10.1.



Figure 31: Schematic view of the Level-1 trigger system of the GLUEX experiment. The electronics boards are described in the text.

Ancillary minimum-bias random trigger and calorimeter LED triggers were col-lected concurrently with data taking.

# 1761 9.3. Performance

The rate of the main physics triggers as a function of the PS trigger rate is 1762 shown in Fig. 32. The typical rate of the PS trigger in spring 2018 was about 1763 3 kHz, which corresponds to a photon beam flux of  $2.5 \cdot 10^7 \gamma$ /sec in the coherent 1764 peak range. The total trigger rate was about 40 kHz. The rates of the random 1765 trigger and each of the LED calorimeter triggers were set to 100 Hz and 10 Hz, 1766 respectively. The electronics and DAQ were running with a livetime close to 1767 100%, collecting data at a rate of 600 MB per second. The trigger system can 1768 operate at significantly higher rates, considered for the next phase of the GlueX 1769 experiment. The combined dead time of the trigger and DAQ systems at the 1770 trigger rate of 80 kHz was measured to be about 10%. The largest contribution 1771 to the dead time comes from the hit processing time of readout electronics 1772 modules. 1773

# 1774 10. Data acquisition

The GLUEX data acquisition software uses the CEBAF Online Data Acquisition (CODA) framework. CODA is a software toolkit of applications and libraries that allows customized data acquisition systems based on distributed commercial networks. A detailed description of CODA software and hardware can be found in Ref. [79].



Figure 32: Rates of the main production triggers as a function of the PS rate: FCAL and BCAL trigger (boxes), BCAL trigger (triangles), the total trigger rate (circles). The vertical arrow indicates the run conditions during the spring of 2018 with a diamond radiator, 5 mm collimator and 75  $\mu$ m Be converter.

The maximum readout capability of the electronics in the VME/VXS crate is 1780 200 MB/s per crate and the number of crates producing data is about 55. The 1781 data from the electronic modules are read via the VME back-plane (2eSST, 1782 parallel bus) by the crate readout controller (ROC), which is a single-board 1783 computer running Linux. The GLUEX network layout and data flow are shown 1784 in Fig. 33. Typical data rates from a single ROC are in the range of 20–70 MB/s, 1785 depending on the detector type and trigger rate. The ROC transfers data over 1786 1 Gbit Ethernet links to Data Concentrators (DC) using buffers containing event 1787 fragments from 40 triggers at a time. Data Concentrators are programs that 1788 build partial events received from 10-12 crates and run on a dedicated computer 1789 node. The DC output traffic of 200-600 MB/s is routed to the Event Builder 1790 (EB) to build complete events. The Event Recorder (ER), which is typically 1791 running on the same node as an Event Builder, writes data to local data storage. 1792 GLUEX has been collecting data at a rate of 500–900 MB/s, which allows the 1793 ER to write out to a single output stream. The system is expandable to handle 1794 higher luminosity where rates rise to 1.5-2.5 GB/s. In this case, the ER must 1795 write multi-stream data to several files in parallel. All DAQ computer nodes 1796 are connected to both a 40 Gb Ethernet switch and a 56 Gb Infiniband switch. 1797 The Ethernet network is used exclusively for DAQ purposes: receiving data 1798 from detectors, building events, and writing data to disk, while the Infiniband 1799 network is used to transfer events for online data quality monitoring. This allows 1800 decoupling DAQ and monitoring network traffic. The livetime of the DAQ is 1801 in the range of 92–100%. The deadtime arises from readout electronics and 1802 depends on the trigger rate. The DAQ software does not cause dead time during 1803 an experimental run, but software-related dead time appears while stopping and 1804 starting the run, which takes between 2-8 minutes. 1805



Figure 33: Schematic DAQ configuration for GLUEX. The high-speed DAQ connections between the ROCs and the ER are contained within an isolated network. The logical data paths are indicated by arrows, although physically they are routed through the 40 Gbit ethernet switch. The online monitoring system uses its own separate 56 Infiniband switch.

Beam Pos	ition and Inte	nsity		Tagger H	Iall			ollimat	or Cave			Hall D	Hall	Status	Beam Pe	mit 1
Location	SCI1 5	CIIA 5-	CIIB	AD00 nA RPM	AD00C BPM	AD00C BCM		Upstre Beam	Profiler	Active Col. Inner	imator Outer	Intensit Monitor	y Tagg	er Status	Beam Pe	mit 1
X position	0.836 mm -0	0- mm 269.	0.538 mm	-0.025 mm	1.225 mm		X posit	tion	.018 mm	0.753 mm	1.255 mm		Lase	r Mode	CW MOD	E (DC)
Y position	3.479 mm	.404 mm	1.030 mm	-0.106 mm	2.508 mm		Y posit	tion 4	1.042 mm	0.361 mm	1.079 mm		Meas	sured Beam Energ	gy 11,385.0	MeV
Current	18.8 nA	16.7 nA	23.5 nA	19.6 nA	15.7 nA	153.0nA	Intens	ity	7,415,063	2.711 V	2.018 V	1,	727 Fast	Feedback Status Shutdown Status	OFF FSD OK	
Magnetic	Elements and	1 Vacuum		Quadrupole		1		1011					HS	S.	olenoid Magnet	_
X corrector	-0.6 Amps		0.3 Amps	Current -4.2 Amps	208.5 Amp	se s		1010	20110	190.0 An	be _	910.0 Amps			1,347.9 Amps	
Y corrector	-0.0 Amps		0.6 Amps	Field	1.4269	F						1.662 G			1.4095 Tesla	
Vaccum	4.9E-7 Torr					2.5E-6 Torr	1	8E-6 Torr	1.1E-6 Torr				4.7E-	6 Torr		
Beamline 501	Devices scrit sc	attos att		Goniometer Positions	]				Collimato	]			Target		ComCal	
Aarp Harp	Viewer H	arp Viewer	X 142.5 mr	m Y 72.0 mm Roll	34.5 deg	hphous Radiator	Pro	filer	×	~	TPOL	PS Converter	Top 4	1.3 K X	7	TAC
osition 11.2 n	nm OUT	7.6 mm OUT	Pitch 0.355	5 deg Yaw 0.774	deg	0.0 mm		0.0 mm	115.3 mm	4.7 mm	70.0 mm	0.0 mm	Bottom 3	4.4 K 0.0 n	nm 134.6 mm	0.0 mm
			Radiator: JD7	70-105 47um 45/135 d	eg PERP	RETRACTED	RETR	ACTED	D = 5.0 m	Ę	Be 75 µm	RETRACTED	EMPTY & F	Ready	RETRACTED	RETRACTED 🔘
1.145 Dates		family file										TAGM Total	PSC Total	DIRC North	BCAL US Total	TOF Total
H <sup>2</sup> SES												79,218,964	18,985	3,415,891	439,085	2,224,856
Tagger 0E0							1	Upstream Be	am Profiler			TAGH Total	PS Total	DIRC South	BCAL DS Total	FCAL Total
Hodoscope	11.35 10.5 10	9.5	8.5 8 7. Photo	5 7 6.5 6 n Energy (GeV)	5.5 5 4.5	4 3.5 2.87	1.64E	T that is				96,885,213	61,257	757,711	462,303	248,213
Ion Chambers at Radiator	e-Halo Counte Tagger	rs Ion Chambe at Magnet	er Ion Cham at Dump	nber y-Halo C Tagger	counters	lon Chamber at y-line	EI FI			y-Halo Cou in Collimate	nters or Cave	PSC Y-H	alo Counters Jpstream Platforn	COMCAL	Intensity	TAC
2.031E3	18			206,	833		1738	70 40 20 BPU )	0 -20 -40 -7 X (mm)	0 1,31	0	Coincidence 2,675	668	10141	MONITOR	
	7,051	9.797	1.8	997E4 168,526	72,063	2.264E3			Ī	2,039	1,799	93	2 - 1,061		0 1.727	4
1.777E3 Tagger Microscope 8.73E5-3	0			147.	568		आ भूम भूम			1,42	-	1.990 PS Coincidence	1,181	6- 4- 2-	7	
Hz 4E5 2E5 0E0 883 8.7	86 85 84 83	82 81 8	at Rad (rad1 2.	diation Probe y-Radii cks at Rach 02_p3) (rad10) 3E-2 mrem/h 1	stion Probe Y-F GS Du 2_p2) .4E-1 mR/H	Radiation Probe imp (rad102_p1) 0.0E0 mrem/h	0E0	-70 -40 -20	7 (mm)	o y-radi cave (rad5i 1.1	ation probe 08_p1) E0 mrem/h	ST 7 984.37	a otra	0- 2- 4- 5 1 1 1 6 4 2 0 -2	-0.5 n-rai hail (radi	ilation probe 08_p2) 0.0E0 mR/H
	Photon Energ	y (GeV)														

Figure 34: Top-level graphical interface for the beamline. This screen provides information on beam currents and rates, radiators, magnet status, target condition, background levels, etc.

## 1806 11. Slow controls

GLUEX must monitor and control tens of thousands of different variables that define the state of the experimental hardware. The values need to be acquired, displayed, archived, and used as inputs to control loops continually with a high degree of reliability. For GLUEX, approximately 90,000 variables are archived, and many more are monitored.

# 1812 11.1. Architecture

The GLUEX slow control system consists of three layers. The first layer 1813 consists of the remote units such as high voltage or low voltage power chas-1814 sis, magnet power supplies, temperature controller, LabView applications, and 1815 PLC-based applications, which directly interact with the hardware and contain 1816 almost the all the control loops. The second layer is the Supervisory Control 1817 and Data Acquisition (SCADA) layer, which is implemented via approximately 1818 140 EPICS Input/Output Controllers (IOCs). This layer provides the inter-1819 face between low level applications and higher level applications via the EPICS 1820 ChannelAccess protocol. The highest level, referred as the Experiment Control 1821 System (ECS), contains applications such as Human-Machine Interfaces, the 1822 alarm system, and data archiving system. This structure allows for relatively 1823 simple and seamless addition and integration of new components into the overall 1824 controls system. 1825

# 1826 11.2. Remote Units

GLUEX uses a variety of commercial units to provide control over the hard-1827 ware used in the experiment. For instance, most detector high voltages are 1828 provided by the CAEN SYx527 voltage mainframe,<sup>58</sup> while the low and bias 1829 voltages are provided by boards residing in a Wiener MPOD chassis<sup>59</sup>. These 1830 two power supply types provide most voltages for detector elements with the 1831 exception of the Tagger Microscope and the Forward Calorimeter. Here custom 1832 systems were developed that provide voltage regulation and interact with the 1833 EPICS-based layer through higher level interfaces using custom protocols. See 1834 Sections 2.4.2 and 7.2 for more details. 1835

Various beam line devices need to be moved during beam operations. Stepper motors are used to move motorized stages via Newport XPS universal multi-axis motion controllers<sup>60</sup> that allow for execution of complex trajectories involving multiple axes. All stage referencing, motion profile computations, and encoder-based closed-loop control occurs within the controller chassis after the basic parameters, such as positions and velocities, are provided by the user via a TCP/IP-based interface to EPICS.

<sup>&</sup>lt;sup>58</sup>https://www.caen.it/subfamilies/mainframes/

 $<sup>^{59} \</sup>rm http://www.wiener-d.com/sc/power-supplies/mpod-lvhv/mpod-crate.html$ 

 $<sup>^{60} \</sup>rm https://www.newport.com/c/xps-universal-multi-axis-motion-controller.$ 

Custom controls were often developed for each complex installation, such 1843 as a superconducting magnet that requires large numbers of input and out-1844 put channels and sophisticated logic. For these cases, we used Allen-Bradley 1845 CompactLogix and ControlLogix PLC systems<sup>61</sup>. These systems are designed 1846 for industrial operations, allow modular design, provide high reliability, and re-1847 quire minimal maintenance. All controls loops are programmed within the PLC 1848 application, and are interfaced with EPICS through a TCP/IP-EtherNet/IP-1849 proprietary protocol to allow access by higher level applications to process vari-1850 ables delivered by the PLCs. 1851

The cryogenic target and the superconducting solenoid employ National In-1852 struments LabView applications. The target controls use both custom-made 1853 and vendor-supplied hardware that include built-in remotely-accessible control 1854 systems and an NI CompactRIO<sup>62</sup> chassis. This chassis communicates with the 1855 hardware and serves variables using an internal ChannelAccess server and an 1856 EPICS IOC running on the CompactRIO controller, as described in Sec. 4. A 1857 National Instruments PXI high-performance system<sup>63</sup> is used to collect data 1858 from different sensors of the solenoid as described in Sec. 3. 1859

# 1860 11.3. Supervisory Control and Data Acquisition layer

The SCADA layer is the middle layer that distributes the process variables 1861 allowing the higher level – and sometimes lower level – applications to use various 1862 process variables of the Hall-D control system. This layer is based on EPICS 1863 and uses the ChannelAccess protocol to publish the values of the variables over 1864 Ethernet. Efficient exchange of the information between the experiment and ac-1865 celerator operations is achieved because the accelerator controls also use EPICS. 1866 Several dozen software IOC processes, running on host computers of the experi-1867 ment control process, collect data from different components of the lowest layer. 1868 Each IOC is configured to communicate using the protocol appropriate for the 1869 remote units with which data exchange is needed. For instance, the IOC con-1870 trolling the voltage for the FDC detector needs to be able to communicate with 1871 the Wiener MPOD and CAEN SYx527 voltage chassis. The middle layer is 1872 primarily used to distribute data between different applications. This layer also 1873 contains some EPICS-based applications running on IOCs that provide differ-1874 ent control loops and software interlocks. For instance, the low-voltage power 1875 supplies for the FDC detector (see Sec. 5.2) are shut off if the temperature or 1876 the flow of the coolant in the chiller falls outside of required limits. 1877

# 1878 11.4. Experiment Control System

<sup>1879</sup> The highest level of controls contains applications that archive data, display <sup>1880</sup> data in interactive GUIs and as stripcharts, alarm and notify shift personnel

<sup>&</sup>lt;sup>61</sup>https://ab.rockwellautomation.com.

<sup>&</sup>lt;sup>62</sup>https://www.ni.com/en-us/shop/compactrio.html

<sup>&</sup>lt;sup>63</sup>https://www.ni.com/en-us/shop/pxi.html

and experts when problems occur, and interface with the CODA-based data ac-1881 quisition system (Sec. 10). An example of such a GUI is the beamline overview 1882 screen, shown in Fig. 34. Many of the buttons of the GUI are active and allow 1883 access to other GUIs. Display management and the alarm system for GLUEX 1884 controls are based on Controls System Studio (CSS),<sup>64</sup> which is an Eclipse-1885 based toolkit for operating large systems. CSS is well suited for systems that 1886 use EPICS as an integral component. Although CSS provides an archiving 1887 engine and stripcharting tools, the MYA archiver, [80] provided by the JLab ac-1888 celerator software group, was employed with its tools for displaying the archived 1889 data as a time-series. Display management for GLUEX controls is within the 1890 CSS BOY [81] environment, which allows system experts to build sophisticated 1891 control screens using standard widgets. The alarm system is based on the CSS 1892 BEAST[82] alarm handler software, which alerts shift personnel of problems 1893 with the detector, and notifies a system expert if the problems are not resolved 1894 by shift personnel. 1895

# 1896 12. Online computing system

<sup>1897</sup> This section describes the GLUEX software and computing systems used for <sup>1898</sup> data monitoring and for transport to the tape system for permanent storage.

# 1899 12.1. Monitoring

The Online Monitoring system consists of multiple stages that provide im-1900 mediate monitoring of the data, as well as near-term monitoring (a few hours 1901 after acquisition). Immediate monitoring is based on the RootSpy system[83] 1902 written for use in GLUEX, though its design is not experiment specific. Fig-1903 ure 35 shows a diagram of the processes involved in the RootSpy system and 1904 how those processes are coupled to the DAQ system. The Event Transfer (ET) 1905 process is part of the CODA DAQ system [84] and is used to extract a copy 1906 of a portion of the datastream without interfering with data acquisition. The 1907 monitoring system uses a secondary ET to minimize connections to the RAID 1908 server running the Event Recorder process. 1909

The monitoring system is run on a small computer farm<sup>65</sup>, with each computer processing a small part of the data stream. In total, about 10% of the data is processed for the low level occupancy plots while roughly 2% is fully reconstructed for higher level analysis. The CODA ET software system is used to distribute the data among the farm computers. Each farm node generates histograms, which *RootSpy* gathers and combines before display to shift workers in a GUI. Plots are displayed via a set of ROOT [85] macros, each responsible

<sup>&</sup>lt;sup>64</sup>http://controlsystemstudio.org/

 $<sup>^{65}</sup>$ The online monitoring farm consists of eight 2012 era Intel x86\_64 computers with 16 cores+16 hyper-threads (ht) plus six 2016 era Intel x86\_64 computers with 36 cores + 36ht. The monitoring farm uses 40 Gbps (QDR) and 56 Gbps(FDR) IB for the primary interconnect. Note that the DAQ system uses a separate 40 Gbps ethernet network that is independent of the farm.



Figure 35: Processes distributed across several computers in the online monitoring system. DC, EB, and ER are the Data Concentrator, Event Builder, and Event Recorder processes, respectively, in the CODA DAQ system.

for drawing a single page. Most macros divide the page into multiple sections so that multiple plots can be displayed on a single page. Figure 36 shows an example of a high-level monitoring plot, where four invariant-mass distributions are shown with fits. Values extracted from the fits are printed on the plots for easy quantitative comparison to a reference plot.

There are several client programs that summarize the information available 1922 in the histograms produced by *RootSpy* and generate output that make it easy to 1923 assess the uniformity and quality of the data. One of these is the RSTimeSeries 1924 program, which periodically inserts data into an InfluxDB time series database. 1925 The database provides a web-accessible strip chart of detector hit rates and 1926 reconstructed quantities (e.g. number of  $\rho$ 's per 1k triggers). Another is the 1927 RSArchiver program that gathers summed histograms to be displayed in the 1928 Plot Browser<sup>66</sup> website. Plot Browser provides easy comparison of plots between 1929 different runs and between different analysis passes. Jobs are automatically 1930 submitted to the JLab farm for full reconstruction of the first five files (100GB) 1931 of each run. The results are displayed in Plot Browser and may be compared 1932 directly with the online analysis of the same run. 1933

# 1934 12.2. Data transport and storage

<sup>1935</sup> GLUEX Phase I generated production data at rates up to 650MB/s. The <sup>1936</sup> data were temporarily stored on large RAID-6 disk arrays, and then copied to

<sup>&</sup>lt;sup>66</sup>https://halldweb.jlab.org/data\_monitoring/Plot\_Browser.html.



Figure 36: Invariant mass distributions showing  $\pi^{\circ}$ ,  $\omega$ ,  $\rho$ , and  $\phi$  particles. These plots were generated online in about 1hr 40min by looking at roughly 2% of the data stream.

	2016	2017	2018
actual (raw data only)	0.624	0.914	3.107
model (raw data only)		0.863	3.172
actual (production data)	0.55	1.256	1.206

Table 4: GLUEX data volumes by year. All values are in petabytes (PB). Most years include two run periods. The line marked "model" gives calculated rates from the GLUEX Computing Model[86] based on the detector luminosity. "Raw data only" represents data generated by the DAQ system (not including the backup copy). "Production" represents all derived data including reconstructed values and ROOT trees.

an LT0 tape system in the JLab Computer Center for long term storage. Two 1937 RAID servers, each with four partitions, were used for staging the data. The 1938 partition being written was rotated between runs to minimize head thrashing 1939 on disks by only reading partitions not currently being written. Partitions were 1940 kept at approximately 80% capacity and older files were deleted to maintain 1941 this level, allowing the monitoring farm easy access to files when the beam was 1942 down. A copy of the first three files (~ 1.5%) of each run was also kept on the 1943 online computers for direct access to samples from each run. 1944

The data volumes stored to tape are shown in Table 4 in units of petabytes (PB). Entries marked "actual" are values taken from the tape storage system. The line marked "model" comes from the GLUEX computing model[86].

### <sup>1948</sup> 13. Event reconstruction

GLUEX uses the computer center batch farm at JLab to perform data mon-1949 itoring, event reconstruction, and physics analyses. For data monitoring, de-1950 tector hit occupancies, calibration and reconstruction quality, and experimental 1951 yields and resolutions, are analyzed for several physics channels. A subset of the 1952 data is monitored automatically as it is saved to tape. Every few weeks, monitor-1953 ing processes are launched on a subset of the data to study improvements from 1954 ongoing calibrations and reconstruction software improvements. The histograms 1955 produced by these monitoring jobs are displayed on a website and ROOT files 1956 are available for download, enabling the collaborators to easily study the quality 1957 of the data. 1958

Every few months, a major reconstruction launch over all of the data is performed, linking hits in the various detector systems to reconstruct particles in physics events. Monitoring plots from these launches are also published to the web. Finally, regular analysis launches over the reconstructed data are performed for the reactions requested by users on a web form. The results of these launches are saved in reaction-specific ROOT TTrees for further analysis.

For all launches, the reconstruction is run in a multi-threaded mode to make efficient use of the available computing resources. Fig. 37 shows the multithreaded scaling from our monitoring launches. The program performs near the theoretical limit for jobs that use a number of threads that is less than or equal to the number of physical cores on the processor. By using hyperthreads, a smaller but still significant gain is achieved. All file outputs are written to awrite-through cache system, which is ultimately backed up to tape.



Figure 37: The scaling of program performance as a function of the number of processing threads. The computer used for this test consisted of 24 full cores (Intel x86\_64) plus 24 hyperthreads. The orange squares are from running multiple processes, each with 12 threads.

GLUEX Phase I has recorded 1400 separate physics-quality runs, with a total data footprint of about 3 petabytes. Data were saved in 19-GB files, with all runs consisting of multiple files (typically 100 or more per run). Fig. 38 shows an overview of the different production steps for GLUEX data, which are described in more detail in the following subsections.

# 1977 13.1. Calibration

During the acquisition of data, a unique run number is assigned to a period 1978 of data corresponding to less than about 2 hours of clock time, which may result 1979 in writing a couple hundred files. It is assumed that the detector changes very 1980 little during this period and therefore there will be no changes in the calibration 1981 constants. Two types of calibration procedures are used, depending on the 1982 complexity of the calibration procedures. Simple, well-understood calibrations 1983 such as timing alignment between individual channels and subdetectors or drift 1984 chamber gain and time-to-distance calibrations, can be performed with one file 1985 1986 of data per run. These procedures are executed either in the online environment or on the batch farm, and can be repeated as needed following any improvements 1987 in reconstruction algorithms or other calibrations. 1988



Figure 38: Production flowchart for GLUEX data, illustrating analysis steps.

More complicated calibration procedures, such as calorimeter gain calibra-1989 tion, require more data and are often iterative procedures, requiring several 1990 passes through the data. The raw data are processed upon arrival on the batch 1991 farm, resulting in histograms or in selected event data files in EVIO [87] or 1992 ROOT-tree format. Many of these outputs require that charged particle tracks 1993 are reconstructed. However, the computationally intensive nature of track re-1994 construction makes it a challenge to fully reconstruct all raw data immediately. 1995 Therefore, the full suite of calibration procedures is only applied to 10 - 20% of 1996 the data. Processing of the remaining data is mostly focused on separating out, 1997 or "skimming," events collected by calibration triggers. 1998

# 1999 13.2. Monitoring

In Fig. 38 the "FULL RAW DATA" box represents experimental data that 2000 have been backed up to tape. The box labeled "subset" represents the first five 2001 files of each run, which are run through offline monitoring processes. These 2002 monitoring jobs are first processed during the run to check the quality of the 2003 data, but are also processed after major changes to calibrations or software to 2004 validate those changes. The resulting Reconstructed Events Storage (REST) 2005 files and ROOT histogram files are used for checking the detector and recon-2006 struction performance. 2007

### 2008 13.3. Reconstruction

When the data have been sufficiently well calibrated, a full (production) pass of the reconstructed software on the physics quality data is performed. In the current total GLUEX data set, about 1400 runs were deemed "physics quality." The remaining runs were short runs related to engineering and commissioning tests of the experiment. The 1400 physics quality runs include the majority of
the data recorded during the running period, representing about 3 petabytes.
All these files were reconstructed using computing resources at several sites,
equivalent to more than 20 million core-hours combined. This produced more
than 500 terabytes of REST data files. The large reduction in size from collected
event data to physics data files (about a factor of six) permits faster and more
efficient physics analyses of the data.

During the REST production, a series of detector studies were performed that required access to raw data and that would not be possible on the reconstructed data alone. Many improvements to software and detector calibration resulted from these studies. Similar studies can be made with simulated data to match and assess the detector acceptance.

# 2025 13.4. Offsite reconstruction

Production processing of GLUEX data uses offsite high-performance com-2026 puting resources in addition to the onsite computing farm at JLab, specifically, 2027 the National Energy Research Supercomputing Center (NERSC) and the Pitts-2028 burgh Supercomputing Center (PSC). For NERSC, the total allocation used for 2029 the academic year 2018-2019 was 53M NERSC units, which was used to process 2030 70.5k jobs. This is equivalent to approximately 9M core-hours on a Intel x86\_64 203 processor. The jobs were run on NERSC's Cori II system, which is comprised of 2032 KNL (Knight's Landing) processors. The PSC allocation was awarded through 2033 the XSEDE<sup>67</sup> allocation system in the last quarter of calendar year 2019 for 5.9 2034 MSU. Only 0.85M SU were used in 2019 to run 7k jobs on the PSC Bridges 2035 system or about 10% of the number processed at NERSC. Figure 39 shows 2036 how the event processing rates scaled with the number of processing threads 2037 for both NERSC and PSC. Jobs run at both of those sites were assigned entire 2038 nodes so the number of processing threads used was equal to the total number 2039 of hardware threads. 2040

Container and distributed file system technologies were used for offsite pro-2041 cessing. The software binaries as well as calibration constants, field maps, etc. 2042 were distributed using the CERN-VM-file system (CVMFS). The binaries were 2043 all built at JLab using a CentOS7 system. A very lightweight Docker con-2044 tainer was made based on CentOS7 that had only a minimal number of system 2045 RPMs<sup>68</sup> installed. All other software, including third-party packages such as 2046 ROOT, were distributed via CVMFS. This meant changes to the container it-2047 self were very rare (about once per year). The Docker container was pulled into 2048 NERSC's Shifter system without modification. The same container was used to 2049 create a Singularity container used at both PSC and on the Open Science Grid 2050 (OSG) for simulation jobs. 2051

2052

Raw data ware transferred from JLab to the remote sites using Globus<sup>69</sup>,

<sup>&</sup>lt;sup>67</sup>https://www.xsede.org.

 $<sup>^{68}\</sup>mbox{RedHat}$  Package Management, https://access.redhat.com/documentation/enus/red\_hat\_enterprise\_linux/5/html/deployment\_guide/ch-rpm

<sup>&</sup>lt;sup>69</sup>https://opensciencegrid.org/technology/policy/globus-toolkit.



Figure 39: Event processing rate versus number of threads for reconstruction jobs on NERSC Cori II (left) and PSC Bridges (right). The slope changes in the NERSC plot are due to the KNL architecture, which had four hardware threads per core. For PSC Bridges, hyper-threading is disabled and the plot shows a single slope.

which uses GridFTP. The Globus tasks were submitted and managed by the SWIF2 workflow tool written by the JLab Scientific Computing group. SWIF2 was needed to manage the data retrieval from tape, for transfer to the remote site, for submission of remote jobs, and for transfer of processed data back to JLab. Disk space limitations at both JLab and the remote sites meant only a portion of the data set could be on disk at any one time. Thus, SWIF2 had to manage the jobs through all stages of data transfer and job submission.

# 2060 13.5. Analysis

The full set of reconstructed (REST) data is too large to be easily handled by individual analyzers. For that reason, a system was developed to analyze data at JLab and extract reaction-specific ROOT trees. This step is represented by the right-hand green box at the bottom of Fig. 38.

Users can specify individual reactions via a web interface. Periodically, the 2065 submitted reactions are downloaded into a configuration file, which steers the 2066 analysis launch. For each reaction, the GLUEX analysis library inside the JANA 2067 framework creates possible particle combinations from the reconstructed parti-2068 cle tracks and showers saved in the REST format. Common selection criteria 2069 are applied for exclusivity and particle identification before performing a kine-2070 matic fit, using vertex and four-momentum constraints. Displaced vertices and 2071 inclusive reactions are also supported. Objects representing successful particle 2072 combinations (e.g.  $\pi^0 \to \gamma \gamma$ ) and other objects are managed in memory pools, 2073 and can be reused by different channels to reduce the overall memory footprint 2074 of the process. With this scheme, up to one hundred different reactions can be 2075 combined into one analysis launch processing the reconstructed data. 2076

<sup>2077</sup> If the kinematic fit converged for one combination of tracks and showers, the <sup>2078</sup> event is stored into a reaction-specific but generic ROOT tree, made accessible <sup>2079</sup> to the whole collaboration. The size of the resulting ROOT trees for the full
data set strongly depends on the selected reaction, but is usually small enough to be copied to the user's home institution for a more detailed analysis.

#### 2082 14. Monte Carlo simulation

The detailed simulation of events in the Hall-D beamline and GLUEX de-2083 tector is performed with a GEANT-based software package. The package was 2084 originally developed within the GEANT3 framework [88] and then migrated 2085 to the GEANT4 framework [89, 90]. The simulation framework uses the same 2086 geometry definitions and magnetic field maps as used in reconstruction. The 2087 geometry includes the full photon beamline, starting at the radiator and ending 2088 at the photon beam dump. Both internal and external event generators are sup-2089 ported by the framework. Internal sources include the coherent bremsstrahlung 2090 source and the single particle gun. Events read from any number of external 2091 generators are also supported. These input events specify one or more primary 2092 vertices to be simulated, which are randomized within the hydrogen target with 2093 timing that matches the RF structure of the beam. 2094

The Monte Carlo data flow is presented in Fig. 40. Events of interest are 2095 generated using either an internal or user-supplied event generator. The in-2096 put event specification is fed to the Hall D GEANT simulation code, either 2097 hdgeant or hdgeant4, which tracks the particles through the experimental setup 2098 and records the signals they produce in the active elements of the detector. 2099 Behavior of the simulation is conditioned by a run number, which corresponds 2100 to a particular set of experimental conditions: beam polarization and intensity, 2101 beamline and detector geometry, magnetic field maps, etc. All this information 2102 is read by the simulation at run-time from the calibrations database, which 2103 functions as the single source for all time-dependent geometry, magnetic field, 2104 and calibration data relevant to the simulation. 2105

Events written by the simulation are processed by the detector response 2106 package *mcsmear*. It applies corrections to the simulated hits to account for 2107 detector system inefficiencies and resolution, and overlays additional hits from 2108 uncorrelated background events. Loss of hits from detector channels, multi-hit 2109 truncation, and electronic deadtime are also applied at this step. Information 2110 needed for this processing comes from the databases for calibrations and run-2111 conditions, and from files containing real backgrounds sampled using random 2112 triggers. Events emerging from the smearing step are deemed to be faithful 2113 representations of what the detector would have produced for the given run in 2114 response to the specified input. These Monte Carlo events are then processed 2115 with the same reconstruction software as used for the real events, and the output 2116 is saved to a REST file. These REST files are then made available for physics 2117 analysis. 2118

# 2119 14.1. Geometry specification

The geometry and material descriptions for the experiment are common across simulation and reconstruction, residing in a family of xml files that follow



Figure 40: The Monte Carlo data flow from event generators through physics analysis REST files. The ovals represent databases containing tables indexed by run number, providing a common configuration for simulation, smearing, and reconstruction. Background events represented by the circle marked *bg* are real events collected using a random trigger, which are overlaid on the simulated events to account for pile-up in the Monte Carlo.

a common schema called the Hall D Detector Specification, or *HDDS* [91, 92].
Run-specific variations of the geometry xml records are maintained in the calibration database. The geometry and magnetic field map are also maintained in the calibration database.

The output events from the simulation are written as a data stream, which may either be piped directly into the next step of the Monte Carlo pipeline or saved to a file. Events are passed between all stages of the Monte Carlo processing pipeline, shown in Fig. 40, using the common data format of the Hall-D Data Model, HDDM [93]. HDDM is used for all intermediate input and output event streams.

# 2132 14.2. Event generators

Simulation starts with the generation of events, which can be specific particles or reactions, or simply unbiased background events. A common toolset has been developed to minimize redundancy. These tools include standard methods to generate the distributions of primary photon beam energies and polarization. An output interface is used to produce files suitable as input to the GEANT simulation.

The photon beam energy distribution can be produced using a coherent 2139 bremsstrahlung generator that accounts for the physical properties of the ra-2140 diator and the photon beamline. This generator allows the user to select the 2141 orientation of the diamond radiator, and then calculates the linear polarization 2142 for each photon. Photons can also be generated according to the spectrum mea-2143 sured in the pair spectrometer during any actual data run by interfacing to the 2144 calibration data base. Here the user inputs the degree of linear polarization and 2145 the orientation. Finally, the user can provide a histogram of the photon energy 2146 spectrum and a second one of the degree of polarization to be used to generate 2147 the photon beam. 2148

One of the first generators was used to simulate the total photoproduction cross section. It is currently used to study backgrounds to physics reactions as well as develop analysis tools for extracting signals. This event generator, called *bggen*, is based on Pythia [94], and includes additions that describe the low-energy photoproduction cross sections. Other generators are tied to specific reactions, where the generator needs to describe the underlying physics.

#### 2155 14.3. HDGEANT

Both GEANT3 and GEANT4 versions are available for simulation of the experiment. Both versions have been tuned to reproduce the behavior of the experiment, but there are some differences arising from how the two versions decide when to stop tracking particles. In general, the simulation mimics the running conditions found across a range of runs, typically a large part of a single run period. The output from GEANT contains both hit times and energies deposited in detector volumes.

#### 2163 14.4. Detector response

Converting time and energy deposits coming from GEANT into electronic 2164 detector responses that match the readout from the experiment is carried out 2165 by the detector response package *mcsmear*. The output of this digitization is 2166 2167 identical to the real data with the exception that the so-called *truth information* about the data is retained to allow detailed performance studies. In addition 2168 to the digitization, at this stage the run-dependent efficiency effects are applied 2169 to the data, including both missing electronic channels and reduced efficiency 2170 of other channels. Additional smearing of some signals is also applied here to 2171 better match the performance of the Monte Carlo to data. 2172

The *mcsmear* package also folds measured backgrounds into the data stream. During regular data collection, random triggers are collected concurrently with data taking (see Section 9). These are separated from the actual data and used to provide experimental background signals in the Monte Carlo, with rates based on the actual beam fluxes in the experiment.

# 2178 14.5. Job submission

A large number of experimental conditions need to be matched in simulated 2179 data. The *MCWrapper* tool was developed to streamline the input specifica-2180 tions, implement consistency with corresponding data reconstruction, seamlessly 2181 access computer offsite resources, and produce Monte Carlo samples in propor-2182 tion to the actual data taken. The goal is to model the differences between runs 2183 and provide a simulated data set, comparable to the real data. The primary 2184 system used for this phase is the Open Science Grid (OSG) in order to lever-2185 age resources in addition to the local JLab computing farm. Many automated 2186 checks are made to avoid flawed submission, and all aspects of the requests and 2187 jobs are monitored during running. Once completed, MCWrapper checks for 2188 expected output files to be returned as if the jobs were run on the JLab farm. If 2189 expected files are not found the system will automatically submit a replacement 2190



Figure 41: Reconstructed mass distributions for the reaction  $\gamma p \rightarrow p \pi^0 \pi^{\pm}(\pi^{\mp})$  for a bin in  $\phi$ . (Left) Distribution of the missing mass off the proton. (Right) Invariant mass distribution for the  $\pi^+\pi^-\pi^0$  system. The blue curves show the resonant contributions, the black curve show the polynomial backgrounds, and the red curve shows the sum. (Color online)

job. Once the jobs are verified completed and all data from the request have been properly moved, the user receives an automated email alerting them that their request has been fulfilled and providing the location where the user can access the event sample.

Users are able to monitor and control their simulations via an online dashboard. The *MCWrapper* dashboard gives information about active projects and allows users (or administrators) to interact with their requests. Users may cancel, suspend, or declare projects complete. Detailed information is presented about the individual jobs, such as where the jobs are being run, basic usage statistics, and current status. This information gives individuals a near realtime look into the production of their Monte Carlo samples.

#### <sup>2202</sup> 15. Detector performance

The capability of the GLUEX detector in reconstructing charged and neutral particles and assembling them into fully reconstructed events has been studied in data and simulation using several photoproduction reactions. The results of these studies are summarized in this section.

# 2207 15.1. Charged-particle reconstruction efficiency

The track reconstruction efficiency was estimated by analyzing  $\gamma p \rightarrow p\omega$ , 2208  $\omega \to \pi^+ \pi^- \pi^0$  events, where the proton, the  $\pi^0$ , and one of the charged pi-2209 ons were used to predict the three-momentum of the other charged pion. Two 2210 methods were used to calculate this efficiency,  $\varepsilon = N_{found} / (N_{found} + N_{missing})$ . 2211 Events for which no track was reconstructed in the predicted region of phase 2212 space contributed to  $N_{missing}$ , while events where the expected track was recon-2213 structed contributed to  $N_{found}$ . For the first method, the  $\omega$  yields for  $N_{found}$ 2214 and  $N_{missing}$  were estimated from the missing mass off the proton; for the sec-2215 ond method, the invariant mass of the  $\pi^+\pi^-\pi^0$  system was used to find  $N_{found}$ . 2216 This analysis was performed for individual bins of track momentum,  $\theta$ , and  $\phi$ . 2217



Figure 42: Tracking efficiency for  $\pi^+$  tracks, determined by data and simulation using two methods. (Color online)

Examples of mass histograms for a typical bin in  $\phi$  are shown in Fig. 41. The exercise was repeated for a sample of  $\omega$  Monte Carlo events. A comparison of the efficiency for pion reconstruction derived from the two methods for both Monte Carlo and experimental data is shown in Fig. 42. The efficiencies for Monte Carlo and experimental data agree to within 5%.

While this reaction only allows the determination of track reconstruction efficiencies for  $\theta < 30^{\circ}$ , this covers the majority of charged particles produced in GLUEX due to its fixed-target geometry. Other reactions are being studied to determine the efficiency at larger angles.

#### 2227 15.2. Photon efficiency

Photon-reconstruction efficiency has been studied using different methods for 2228 the FCAL and BCAL. In the FCAL, absolute photon reconstruction efficien-2229 cies have been determined using the "tag-and-probe" method with a sample 2230 of photons from the reaction  $\gamma p \to \omega p, \, \omega \to \pi^+ \pi^- \pi^0, \, \pi^0 \to \gamma(\gamma)$ , where one 2231 final photon is allowed but not required to be reconstructed. The yields with 2232 and without the reconstructed photon are determined using two methods. In 2233 the first method, the  $\omega$  yield is determined from the missing-mass spectrum, 2234  $M_X(\gamma p \to pX)$ , selecting on whether only one or both reconstructed photons 2235 are consistent with a final-state  $\pi^0$ . In the second method, the count when both 2236 photons are found is determined from the  $\omega$  yield from the fully reconstructed 2237 invariant mass  $M(\pi^+\pi^-\gamma\gamma)$ . If the photon is not reconstructed, the  $\omega$  yield 2238 is determined by a fit to the distribution of the missing mass off the proton. 2239 Both methods yield consistent results, with a reconstruction efficiency generally 2240 above 90%, and within 5% or less agree with the efficiencies determined from 2241 simulation. 2242

A relative photon efficiency determination has been performed using  $\pi^0 \rightarrow \gamma\gamma$  decays, which spans the full angular range detected in GLUEX. A sample of fully reconstructed  $\gamma p \rightarrow \pi^+ \pi^- \pi^0 p$  events were inspected, taking advantage of the  $\pi^0 \rightarrow \gamma\gamma$  decay isotropy in the center-of-mass frame. Thus, any anisotropy indicates an inefficiency in the detector. Results from this analysis are illustrated



Figure 43: Photon reconstruction efficiency in FCAL determined from  $\gamma p \rightarrow \omega p$ ,  $\omega \rightarrow \pi^+\pi^-\pi^0$ ,  $\pi^0 \rightarrow \gamma(\gamma)$  as a function of (left) photon energy and (right) photon polar angle. Good agreement between data and simulation is observed in the fiducial region  $\theta = 2^\circ - 10.6^\circ$ . (Color online)



Figure 44: Ratios of relative photon reconstruction efficiency between data and simulation determined from  $\pi^0 \to \gamma \gamma$  decays in  $\gamma p \to \pi^+ \pi^- \pi^0 p$  events. The efficiency ratios are shown for the cases where (left) both photons were measured in the BCAL, (middle) both photons were measured in the FCAL, and (right) one photon was measured in the BCAL and the other in the FCAL.

in Fig. 44. Generally, this relative efficiency is above 90%, and agrees within 5% of that determined from simulation.

The models for the simulated response of both calorimeters are being updated, and the final agreement between photon efficiency determined in data and simulation is expected to improve.

Detailed studies of detector performance determined the standard fiducial region for most analyses to be  $\theta = 2^{\circ} - 10.6^{\circ}$  and  $\theta > 11.3^{\circ}$ . These requirements avoid the region dominated by beam-related backgrounds at small  $\theta$  and the transition region between the BCAL and FCAL, where shower reconstruction is difficult.

# 2258 15.3. Kinematic fitting

Kinematic fitting is a powerful tool to improve the resolution of measured data and to distinguish between different reactions. In GLUEX, this method takes advantage of the fact that the initial state is very well known, with the

target proton at rest, and the incident photon energy measured with very high 2262 precision (< 0.1%). This knowledge of the initial state gives substantial im-2263 provements in the kinematic quantities determined for exclusive reactions. The 2264 most common kinematic fits that are performed are those that impose energy-2265 momentum conservation between the initial and final-state particles. Additional 2266 optional constraints in these fits are for the four-momenta of the daughters of 2267 an intermediate particle to add up to a fixed invariant mass, and for all the 2268 particles to come from a common vertex (or multiple vertices, in the case of 2269 reactions containing long-lived, decaying particles). 2270

To illustrate the performance of the kinematic fit, we use a sample of  $\gamma p \rightarrow \gamma p$ 2271  $\eta p, \eta \to \pi^+ \pi^- \pi^0$  events selected using a combination of standard particle iden-2272 tification and simple kinematic selections. The use of the kinematic fit im-2273 proves the  $\eta$ -mass resolution from 2.6 MeV to 1.7 MeV, which is typical of 2274 low-multiplicity meson production reactions. The quality of the kinematic fit is 2275 determined using either the probability calculated from the  $\chi^2$  of the fit and the 2276 number of degrees-of-freedom or the  $\chi^2$  of the fit itself. The distributions of the 2277 kinematic fit  $\chi^2$  and probability are illustrated in Fig. 45 for both reconstructed 2278 and simulated data. The agreement between the two distributions is good for 2279 small  $\chi^2$  (large probability), and flat over most of the probability range, indicat-2280 ing good overall performance for most signal events. The disagreement between 2281 the two distributions at larger  $\chi^2$  (probability < 0.2) is due to a combination of 2282 background events and deficiencies in the modelling of poorly measured events 2283 with large resolution. 2284

The performance of the reconstruction algorithms and kinematic fit can be studied through investigating the "pull" distributions, where the pull of a variable x is defined by comparing its measured values and uncertainties and those resulting from the kinematic fit as

$$\operatorname{pull}_{x} = \frac{x_{\operatorname{fitted}} - x_{\operatorname{measured}}}{\sqrt{\sigma_{x,\operatorname{measured}}^{2} - \sigma_{x,\operatorname{fitted}}^{2}}}.$$
(1)

If the parameters and covariances of reconstructed particles are Gaussian, are measured accurately, and the fit is performing correctly, then these pull values are expected to have a Gaussian distribution centered at zero with a width  $\sigma$ of 1. If the pull distributions are not centered at zero, this is an indication that there is a bias in the measurements or the fit. If  $\sigma$  varies from unity, this is an indication that the covariance matrix elements are not correctly estimated.

As an example, the pull distributions for the momentum components of 2295 the  $\pi^-$  in reconstructed  $\gamma p \to \eta p$ ,  $\eta \to \pi^+ \pi^- \pi^0$  events are shown in Fig. 46. 2296 Both real and simulated data have roughly Gaussian shapes with similar widths. 2297 More insight into the stability of the results of the kinematic fit can be found 2298 by studying the variation of the means and widths of the fit distributions as 2299 a function of the fit probability. The results of such a study are summarized 2300 in Fig. 47, where broad agreement between the results from real and simulated 2301 data is seen. The means of the pull distributions are generally around zero, 2302 except for  $p_x$  with a mean of roughly -0.1, and the widths within about 20% of 2303



Figure 45: Distribution of kinematic fit (left) probability and (right)  $\chi^2$  for reconstructed  $\gamma p \rightarrow \eta p, \eta \rightarrow \pi^+ \pi^- \pi^0$  events in data and simulation. Both distributions agree reasonably for well-measured events, and diverge due to additional background in data and differences in modeling poorly-measured events. (Color online)



Figure 46: Pull distributions for momentum components of the  $\pi^-$  from reconstructed  $\gamma p \to \eta p, \eta \to \pi^+ \pi^- \pi^0$  events in data and simulation for events with fit probability > 0.01: (left)  $p_x$ , (center)  $p_y$ , (right)  $p_z$ . (Color online)

<sup>2304</sup> unity. This level of performance and agreement between data and simulation is <sup>2305</sup> acceptable for the initial analysis of data, where very loose cuts on the kinematic <sup>2306</sup> fit  $\chi^2$  are performed, and steady improvement in the modeling of the covariance <sup>2307</sup> matrices of reconstructed particles is expected to continue.

#### 2308 15.4. Invariant-mass resolution

The invariant-mass resolution for resonances depends on the momenta and 2309 angles of their decay products. This resolution has been studied using several 2310 different channels, which are illustrated in Figs. 48 and 50. A typical meson 2311 production channel including both charged particles and photons,  $\omega \to \pi^+ \pi^- \pi^0$ 2312 from  $\gamma p \rightarrow \omega p$ , is shown in the left panel of Fig. 48. The distribution shows 2313 the strong peak due to  $\omega$  meson production. Other structures are also seen, 2314 such as peaks corresponding to the production of  $\eta$  and  $\phi$  mesons. The  $\omega$  peak 2315 resolution obtained is 26.1 MeV when using only the reconstructed particle 4-2316 vectors, and improves to 16.4 MeV after a kinematic fit. The invariant-mass 2317 distribution of  $\pi^+\pi^-$  from  $\gamma p \to K_S K^+\pi^- p$ ,  $K_S \to \pi^+\pi^-$  exhibits the peak 2318 due to  $K_S \to \pi^+\pi^-$  decays (right panel of Fig. 48). The  $K_S$  peak resolution is 2319 17.0 MeV using only the reconstructed charged particle 4-vectors, and improves 2320 2321 to 8.6 MeV after a kinematic fit imposing energy and momentum conservation.



Figure 47: Pull means (top) and sigmas (bottom) for the momentum components of each particle as a function of the minimum probability required of the fit from reconstructed  $\gamma p \rightarrow \eta p, \eta \rightarrow \pi^+ \pi^- \pi^0$  events. (Color online)



Figure 48: (Left)  $\pi^+\pi^-\pi^0$  invariant-mass distribution from  $\gamma p \to \pi^+\pi^-\pi^0 p$  (Right)  $\pi^+\pi^-$  invariant mass distribution from  $\gamma p \to K_S K^+\pi^- p$ ,  $K_S \to \pi^+\pi^-$ . (Color online)



Figure 49:  $K_S \rightarrow \pi^+\pi^-$  invariant mass resolution for the events shown in Fig. 48, as a function of  $K_S$  momentum, both before and after a kinetic fit, which constrains energy and momentum conservation. (Color online)

The dependence of the  $K_S \to \pi^+\pi^-$  invariant-mass resolution as a function of  $K_S$  momentum is shown in Fig. 49, both before and after an energy/momentumconstraint kinematic fit.

The invariant mass of  $\Lambda^0 \pi^-$  from  $\gamma p \to K^+ K^+ \pi^- \pi^- p$  is shown in the left 2325 panel of Fig. 50, illustrating the peak due to  $\Xi^- \to \pi^- \Lambda^0$ ,  $\Lambda^0 \to p\pi^-$ . The  $\Xi^-$ 2326 peak resolution obtained is 7.3 MeV when using only the reconstructed charged 2327 particle 4-vectors, and improves to 4.6 MeV after a kinematic fit imposing en-2328 ergy and momentum conservation and the additional constraint that the mass 2329 of the  $p\pi^-$  pairs must be that of the  $\Lambda^0$  mass. The  $e^+e^-$  invariant mass distri-2330 bution from kinematically fit  $\gamma p \rightarrow e^+e^-p$  events is shown in the right panel of 2331 Fig. 50, illustrating the peak due to  $J/\psi \rightarrow e^+e^-$ . The resolution of the peak is 2332 13.7 MeV. 2333

# 2334 15.5. Particle identification

Particle identification in GLUEX uses information from both energy loss indifferent detector systems and time-of-flight measurements. This information



Figure 50: (Left)  $\Lambda^0 \pi^-$  invariant mass distribution from  $\gamma p \to K^+ K^+ \pi^- \pi^- p$ . (Right)  $e^+ e^-$  invariant mass distribution from kinematically fit  $\gamma p \to e^+ e^- p$  events. (Color online)

can be used for identification in several ways. The simplest method is to apply selections directly on the relevant PID variables. To include detector resolution information, one can create a  $\chi^2$  variable comparing a measured value to the expected value for a particular hypothesis, that is

$$\chi^{2}(p) = \left(\frac{X(\text{measured}) - X(\text{expected})_{p}}{\sigma_{X}}\right)^{2}$$
(2)

where X is the given PID variable, p is the particle hypothesis, and  $\sigma_X$  is the resolution of this variable. Multiple PID variables can be combined into one probability, or a figure-of-merit. Standard, loose selections on time-of-flight and energy loss are sufficient for initial physics analyses, while the performance of more complicated selections is being actively studied.

At sufficiently large  $\theta$ , the energy loss for charged particles in the central drift chamber dE/dx can be used. Fig. 51 illustrates these distributions for positively charged particles, showing a clear separation of pions and protons in the momentum range  $\lesssim 1$  GeV. The dE/dx resolution is approximately 27%, with the separation between the pion and proton bands dropping from about  $8\sigma$ at p = 0.5 GeV/c to about  $2\sigma$  at p = 1.0 GeV/c, with both bands fully merged by p = 1.5 GeV/c.

The primary means of particle identification is through time-of-flight mea-2353 surements, and information from several sources is combined to make the most 2354 accurate determination. The RF reference signal from the accelerator is used to 2355 define the time when each photon bunch enters the target. The reconstructed 2356 final-state particles are used to determine which photon bunch most likely gen-235 erated the detected reaction, with the primary determination coming from the 2358 signals from the Start Counter associated with the charged particle tracks. The 2359 photon bunch determination has a resolution of < 10 ps. Each charged par-2360 ticle is associated with additional timing information based on the hit in the 236 highest resolution detector (for example the BCAL or TOF). The flight time 2362 to this measured hit  $t_{\text{meas}}$  relative to the time of the photon bunch that gen-2363 erated the event  $t_{\rm RF}$  can be used to distinguish between particles of different 2364 mass. Two common variables that are used are the velocity  $(\beta)$  determined 2365



Figure 51: CDC energy loss (dE/dx) for positively charged particles that have at least 20 hits in the detector, as a function of measured particle momentum. The band corresponding to protons curves upwards, showing a larger energy loss than pions and other lighter particles at low momentum. The two bands show a clear separation for momenta  $\leq 1$  GeV. A faint kaon band can be seen between them.



Figure 52: Resolution as a function of particle momentum for  $\Delta t_{\rm RF}$  in various subdetectors: (left) BCAL, (center) FCAL, (right) TOF (Color online)

using the measured time-of-flight and the momentum of the particle, and  $\Delta t_{\rm RF}$ . 2366 the difference between the measured and RF times after they both have been 2367 extrapolated back to the center of the target, assuming some particle-mass hy-2368 pothesis. An example of the separation between different particle types can be 2369 seen in Fig. 29. The loose selections used for initial analyses of this data placed 2370 on the  $\Delta t_{\rm RF}$  distributions and the momentum dependence of the resolution of 2371 this variable in different detectors are shown in Fig. 52. Requiring reconstructed 2372 particles to have  $\Delta t_{\rm RF} \lesssim 1-2$  ns has been found to be sufficient for analyses 2373 of high-yield channels which are the focus of initial analysis. The study of the 2374 selections required for more demanding channels is ongoing. 2375

Electrons are identified using the ratio of their energy loss in the electromagnetic calorimeters E to the momentum reconstructed in the drift chambers p. This E/p ratio should be approximately unity for electrons and less for hadrons. The overall distributions of this variable are illustrated in Fig. 53. Other variables, such as the shape of the showers generated by the charged particles in the calorimeter, promise to provide additional information to separate electron



Figure 53: Electron identification in the calorimeters is performed using the E/p variable, the ratio of the energy loss in the electromagnetic calorimeters (E) to the momentum reconstructed in the drift chambers (p). Left) This distribution was obtained using  $e^{\pm}$  showers reconstructed in the FCAL from the reaction  $\gamma p \to \pi^0 p$ ,  $\pi^0 \to e^+ e^- \gamma$ . Right)  $e^{\pm}$  showers reconstructed in the BCAL from photon conversions.

2382 and hadron showers.

# 2383 16. Summary and outlook

We have presented the design, construction, and performance, of the beam-2384 line and detector of the GLUEX experiment in Hall D at Jefferson Lab during 2385 its first phase of operation. The experiment operated routinely at an incident 2386 photon flux of  $2 \times 10^7$  photons/s in the coherent peak with an open trigger, 2387 taking data at 40 kHz, and recording 600 MB/s to tape with live time >95%. 2388 During this period the experiment accumulated  $121.4 \text{ pb}^{-1}$  in the coherent peak 2389 and 319.4 pb<sup>-1</sup> total for  $E_{\gamma} > 8.1$  GeV. Data were collected in two sets of or-2390 thogonal linear polarizations of the incident photons, with  $\sim 23\%$  of the data in 2391 each of the four orientations. The remaining  $\sim 11\%$  was collected with unpolar-2392 ized photons. Approximately 270 billion triggers were accumulated during this 2393 period, as shown in Fig. 54. 2394

The operational characteristics of the charged and neutral particle detectors, 2395 trigger, DAQ, online and offline systems have been verified, and individual com-2396 ponents performed as designed. The detector is able to reconstruct exclusive 2397 final states, reconstruction efficiencies have been determined, and Monte Carlo 2398 simulations compare well with experimental data. The infrastructure is in place 2399 to process our high volume of data both on the JLab computing farm as well 2400 on other offsite facilities, providing the ability to process the data in a timely 2401 fashion. 2402

Future running will include taking data at higher luminosity and with improved particle identification capability. The GLUEX experiment has already implemented the necessary infrastructure to allow the experiment to operate at a flux of  $5 \times 10^7$  photons/s in the coherent peak for the upcoming run periods



Figure 54: Plot of integrated number of triggers versus the number of live days in 2017 and 2018. The legend provides the number of triggers for the four diamond orientations relative to the horizontal  $(0, 45, 90, 135^{\circ})$  and the amorphous radiator. The trigger curves of the four diamond configurations fall on top of one another, as we attempted to match the amount of data taken for each configuration. (Color online)

and has added a new DIRC detector<sup>70</sup> to extend particle identification of kaons
 to higher momenta.

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<sup>&</sup>lt;sup>70</sup>Four "bar boxes" from the BaBar DIRC[95] detector have been installed and tested.

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